





Repeatability comparison of conventional mounting technique using facebow and virtual mounting technique based on cone beam computed tomography

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ABSTRACT

Repeatability comparison of conventional mounting technique using facebow and virtual mounting technique based on cone beam computed tomography

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The introduction of digital technology in dentistry has led to the shifting of conventional methods to digital techniques. However, it is challenging to place a digitized dental model to a virtual articulator. To transfer the patient's location information to the virtual articulator, conventional mounting must be performed to the real patient using an anatomic facebow then scan it with a tabletop scanner and transfer it to the virtual articulator. But this process is complicated and inconvenient. Several techniques are available to resolve such problems, yet, they are not definite methods, and digitized dental models are often placed arbitrarily on a virtual articulator.

If cone beam computed tomography (CBCT)'s field of view is broad, the location information of the head and neck structures can be obtained. Therefore, this study presents the virtual mounting technique (VM) using virtual facebow based on CBCT and the



conventional mounting technique (CM) using anatomic facebow and compare the repeatability precision of those two techniques. The null hypothesis of this study is there is no difference between the CBCT based VM and the anatomic facebow based CM.

The experimental group was divided into CM and VM group. A reference articulator was fabricated by scanning a semi-adjustable articulator (Hanau Modular Articulator System, Whip Mix Corp., Louisville, KY, USA) using an industrial scanner (C500, Solutionix, Seoul, Korea). For the CM group, the conventional mounting was performed using an anatomic facebow (Indirect Spring Bow, Waterpick, Buffalo, NY, USA), the articulator was scanned with an industrial scanner and located to the same position as the reference articulator. For the VM group, the CBCT (ASAHI Alphard 3030[®] Belmont Takara., Kyoto, Japan) image was converted to skull standard tessellation language (STL) format on cad software (Exocad cad software, ExocadGmbH, Darmstadt, Germany), then the skull was placed to the reference articulator by using a virtual facebow scanned with an industrial scanner. For both CM and VM, each of the representative model was placed on the reference articulator by using superimposed medium (CM-mounted cast, VM-skull), target points were set for #11, 16, 26 teeth in reverse engineering software (Geomagic Control X, OR3D Ltd., Chirk, UK), and the X, Y, Z coordinate values were obtained in the three-dimensional spatial coordinates.

To analyze the difference between CM and VM, comparative analysis was performed on the four aspects: average distance between the target points, standard deviation of target points for each axis, the spatial relationship between each technique for the X, Y, Z-axis of



tooth #11, and angle of the occlusal plane. A Kolmogorov-Smirnov test was performed to determine normality and paired t-test was conducted if variables followed a normal distribution, otherwise, a Wilcoxon signed-rank test was conducted.

The average distance between the predetermined target points was significantly greater in CM compared with the VM (P<0.01). Also, in CM, the standard deviation between the target points was more than VM (P<0.05). Especially, Z-axis (upward and downward) in CM showed a tendency for high standard deviation compared to other axes. In terms of tooth #11, VM was located more forward than CM (P<0.01), and there was a tendency of CM to be positioned higher than VM in one out of five repetitions (20%, P<0.05). The angle of the occlusal plane was significantly steeper in CM (P<0.001).

Based on the results of four analysis methods, VM shows higher precision than CM in terms of the average distance and the standard deviation. The cast mounted with VM positioned ahead of the cast mounted with CM. And the angle of the occlusal plane of CM tended to be steeper than VM. Further studies are required to verify the clinical usefulness.

Key words: CBCT virtual mounting, comparison of conventional mounting and virtual mounting, digital dentistry, direct digital method, virtual articulator, virtual facebow, virtual mounting technique



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1. INTRODUCTION

One of the most important components in prosthodontic treatment is how precisely dentists can reproduce patient's oral environment. The maxillary model for fabricating a prosthesis should correspond to the movements of mandibular condyle, and mounted in the same position as the actual patient, while considering aesthetic factors, such as midline, anterior occlusal plane, etc^{1, 2}. A facebow is an diagnostic instrument used for registration of the spatial position of maxilla against the cranial base to the articulator using anatomic reference points (GPT-9)³. It can reproduce anterior-posterior position of the cast against condyle that resembles the actual patient condition, and has ability to register horizontal relationships more accurately compared with the arbitrary mounting so that occlusal plane



can be reproduced in articulator similar to the actual condition⁴. Facebow transfer is an essential procedure in prosthodontic treatment⁵⁻⁷ but dentists who are not used to it often encounter difficulties in the actual clinical practice; they may not handle the instrument properly or make the patient uncomfortable while positioning the earplug into the external auditory meatus, and inevitably consume more time⁸. The standard transferring procedure cannot be applied in maxillofacial deformity⁹, and, there has been constant controversy over its precision¹⁰⁻¹².

Recent advances in digital devices such as computer-aided design and computer-aided manufacturing (CAD/CAM), and intraoral scanner is causing many changes in the dentistry field^{13, 14}. The method of manufacturing the computer-aided crown was first presented in the late 80s¹⁵, in the following year, starting with the fabrication of the chairside crown using CAD/CAM system¹⁶ most of the existing conventional technique is being replaced by digital technique. This has changed the workload, facilitated the retention of information on the final prosthesis and reproduction of the prosthesis. To place digitized dental model to virtual articulator, perform conventional mounting using anatomic facebow, scan it to tabletop scanner and transfer it to virtual dental space (Indirect digital method), or use intraoral scanner to implement total arch scanning, and then transfer it to virtual articulator by virtual facebow technique (Direct digital method) (Figure 1)^{17, 18}. To use the indirect method, the mounting process on a mechanical articulator should be preceded, which is inconvenient and complicated. Various direct methods are available to compensate for these issues, such as utilizing standardized extraoral photograph¹⁹, 3-dimensional (3D) optical



scanner²⁰⁻²³, digital axiography²⁴, switching to 3D face scan by continuous photographing ²⁵, stereophotogrammetry²⁶, cone beam computed tomography (CBCT)²⁷⁻²⁹, cephalometric image^{30, 31} etc. However, so far, there is no definite method.

| Analog Method | Indirect Digital Method | Direct Digital Method | |
|--------------------------------|------------------------------------------------|--------------------------------------------|--|
| Conventional impression taking | | Taking improvion and | |
| Bite registration | | inter-occlusal record through intraoral | |
| Definit | ive cast | - scanner | |
| Mechanical fa | cebow transfer | Virtual facebow | |
| Mounting of maxillary cast | | Superimposition of data in virtual dental | |
| Mounting of mandibula | r cast with bite material | space | |
| | Indirect digital scan with tabletop scanner | | |
| | Transfer data to virtual dental space | | |
| | Digitized cast mounte | d on virtual articulator | |

Figure 1. Schematic diagram for transferring patient information to articulator. There is no definite method for transferring the digitized dental model to virtual articulator in the process of direct digital method (dark violet).



CBCT is a radiological tool for diagnosis and provides information on the position of maxilla against the cranial base, bilateral condyle, teeth, soft tissues, and their relationships. One drawback is that the patient is unavoidably exposed to radiation during CBCT imaging, however, it can be used as a medium for transferring the digitized dental model to the virtual articulator because it can identify the relationship between anatomical structures existing in the maxillofacial area in a single shot. Due to these features, a virtual patient was reproduced by overlapping CBCT images and stereophotogrammetric images obtained by an intraoral and facial scanner³², a virtual facebow transfer technique using CBCT which set up the Bergstorm point as an arbitrary posterior reference point had presented²⁹.

If CBCT's field of view of is broad, the location information of head and neck anatomical structures can be obtained. Therefore, the purpose of this study is to present a digital facebow transfer technique based on CBCT and resolve any inconveniences occurring during the transfer of the existing digitized dental model onto virtual dental space. Also, the study aimed to evaluate the usefulness of the virtual mounting technique (VM) in real clinical practice by performing comparative analysis on the repeatability of the conventional mounting technique (CM) using anatomic facebow and virtual mounting technique using CBCT based virtual facebow along with the difference in the degree of an error. The null hypothesis of this study is there is no difference between the CBCT based VM and the anatomic facebow based CM.



2. MATERIALS AND METHODS

Before explaining the flow of this study in detail, a simple schematic diagram is presented (Figure 2).





Figure 2. Schematic diagram of this study



2.1. Selection of research subjects

The subject of the study was patients who were vulnerable and visited the Prosthodontic department of Yonsei University Dental hospital for one year after IRB registration (2-2019-0014). A total of 15 subjects were recruited based on precedent research involving human subjects, which performed a comparative analysis between conventional technique and virtual technique³³. For patients agreeing to participate in the study, they were given an explanation of the purpose and method of the study, and written consent was prepared with the subject. The inclusion and exclusion criteria for selecting the subjects are as are listed on Table 1³⁴⁻³⁶. If a candidate met inclusion criteria, the person was selected as a subject of the study, and maxillary study impressions were taken five times with an alginate (Aroma fine plus normal set, GC, Tokyo, Japan). Then, five of the same model of facebow (Indirect Spring Bow, Waterpick, Buffalo, NY, USA) can be prepared, and one operator (K.S.J) performs facebow transfer five times without pause (Figure 3). The idea of repeating five times on 15 study subjects is based on the precedent research²⁶. After that, CBCT (ASAHI Alphard 3030[®] Belmont Takara., Kyoto, Japan) was performed. P mode (exposure area of 15.4mm x 15.4mm, 0.3/voxel (mm), effective dose of 350.0±0.38 μSv,) was used for CBCT's field of view (FOV) to reproduce subject's anatomical structures including maxilla, infraorbital point, bilateral external acoustic pore (porion), and condylar components. The image is exported to digital imaging and communications in medicine (DICOM) file.



`

Table 1. Inclusion and exclusion criteria for selection subjects

| Men and women over 19 years of age whose occlusion need to be analyzed before proceeding with Subjects with history temporomandibular joint disord and jaw related surgery. | Inclusion criteria | Exclusion criteria |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| (2) Subjects with one or fewer metal prosthesis or a restoration in a quadrant that may cause scattering during CBCT imaging process. (3) Subjects with one or fewer missing tooth in a quadrant. (4) Subjects with four of fewer dental prosthesis (5) Subjects who signed the written consent. (2) Severe facial asymmetry maxillofacial deformity. (3) Subjects with systemic disea who are unable to receive routi dental treatment. (3) Subjects devoid of men capacity. (4) Subjects with four of fewer dental prosthesis (5) Subjects who signed the written consent. | Men and women over 19 years of age whose occlusion need to be tempor analyzed before proceeding with prosthodontic treatment. Subjects with one or fewer metal prosthesis or a restoration in a quadrant that may cause scattering during CBCT imaging process. Subjects with one or fewer missing tooth in a quadrant. Subjects with four of fewer dental prosthesis Subjects who signed the written consent. | ets with history of comandibular joint disorder w related surgery. e facial asymmetry or ofacial deformity. ets with systemic disease re unable to receive routine treatment. ets devoid of mental ty. ant women. |





Figure 3. Facebow transfer for the conventional mounting. One operator repeats 5 times without pause using 5 identical facebows.



2.2. Experimental design

2.2.1. Production of the Reference articulator library

Five cubic shaped resin markers (Z100, 3M ESPE, St Paul, MN, USA; size: 2mm x 2mm) were attached on semi-adjustable articulator (Hanau Modular Articulator System, Whip Mix Corp., Louisville, KY, USA). The whole articulator was scanned with a high-resolution industrial scanner (C500, Solutionix, Seoul, Korea) that shows 10µm accuracy according to the manufacturer's manual. Calibration was performed on articulator according to the manufacturer's instructions and object holder was used to prevent unwanted movements of articulator during scanning. Also, powder spray (Dr. MAT 3D SCAN WHITE SPRAY PSCS-01, Dr. MAT, Istanbul, Turkey) was applied onto the articulator to prevent diffused reflection that can occur in articulator during the procedure. The overall quality of scanned data was checked, and it was converted into standard tessellation language (STL) format using software (ezSCAN 2017, solutionix, Seoul, Korea) to be used in CAD software (Exocad cad software, ExocadGmbH, Darmstadt, Germany) (Figure 4). The articulator STL file made as such is called a "**Reference articulator**", which will be used as a reference for all the superimpositions performed in this study.





Figure 4. The Reference articulator. Resin markers were attached on the articulator to facilitate superimposition (Yellow arrows).



2.2.2. Conventional mounting procedure

The process for collecting the CM data is as follows/

- (1) Five study models for each study subject were fabricated by mixing type III improved dental stone (MG Hi-Koseton, Maryushi Gypsum Co.Ltd. Osaka, Japan) according to manufacturer's mixing ratio (plaster 100g/water 24cc) and by pouring it into the obtained alginate impressions. Since there is a total of 15 subjects, a total of 75 study models were prepared. One model with the least defects was selected and was converted into STL format with a tabletop scanner (Identica Blue, Medit Co., Seoul, Korea). This is called the "Representative model" for each subject.
- ② Mounting was performed on real Reference articulator by using five facebows that recorded the relationship of maxilla against the subject's cranial base. The study models fabricated in step ① were mounted by mixing type II dental plaster (Silky Gemma, SAMWOO CO., LTD, Seoul, Korea) according to the manufacturer's mixing ratio (plaster 100g/water 40cc). As there were 15 subjects, the mounting was performed a total of 75 times, five times each for a subject. At this time, the articulator was limited to only one real articulator which fabricated the Reference articulator in 2.3.1 (Figure 5).
- ③ 75 maxillary study models fabricated in ② mounted on an articulator were scanned with an industrial scanner C500 while replacing the mounting plate (Figure 6). Before scanning, powder spray was applied to the surface of articulator to





Figure 4. Conventional mounting on the Reference articulator using a mechanical facebow





Figure 5. Scanning of conventional mounting models using the industrial scanner. Powder spray was applied to the surface of articulator to prevent diffused reflection that may occur during scanning.



prevent diffused reflection that may occur during scanning. The file was converted into STL format with software ezSCAN 2017 to be used in Exocad software (Figure 7). These 75 STL files are called the **"Conventional mounting model**". Since Conventional mounting model will be superimposed on the Reference articulator file in the future, an attention was focused on scanning the upper part of articulator where the model is attached (Figure 8A).

④ The STL file of the Reference articulator and Conventional mounting model were imported to Exocad cad software and Conventional mounting model was superimposed over the Reference articulator file through a best-fit algorithm using a resin marker attached to the articulator (Figure 8B). If the Representative model fabricated in ① is superimposed over the maxilla of Conventional mounting model (Figure 8C), the Representative model having location information mounted on Reference articulator can be obtained (Figure 8D). This procedure was repeated five times and the data of the conventional mounting technique was prepared (Figure 8E, 8F).





Figure 6. Scanning process using ezSCAN 2017, a software dedicated to scanning





Figure 7. The process for collecting the CM data. A. Scanned Conventional mounting model. B. Superimposition of scanned conventional mounting model(yellow) to the Reference articulator(Grey) C. Superimposition of the subject's representative model(violet) D. Mounted Representative model on the Reference articulator. E. Five identical Representative models mounted on the Reference articulator. F. Aligned STL files with the current locational information.



2.2.3. Virtual mounting procedure

The process for collecting VM data is as follows.

- (1) Attach the facebow to the real Reference articulator and scan the upper part of the articulator and facebow with an industrial scanner. This scan file is called "**Digitized facebow**". Import the Reference articulator and Digitized facebow file to Exocad software and superimpose the Digitized facebow over the Reference articulator using resin markers. Since all of the Conventional mounting models prepared earlier are aligned with the locational information of the Reference articulator so that the locational information of the Reference articulator so that the locational information of the Reference articulator so that the locational information of the Reference articulator does not change (Figure 9).
- ⁽²⁾ Import the DICOM file of CBCT on Exocad software and convert it into a 3D model through the DICOM viewer and export it to the STL file. At that time, complete the morphology of the skull by controlling the surface threshold so that one can identify both the external acoustic meatus and minimize the artifacts due to dental restorations (Figure 10A).
- ③ Align the skull file into Digitized facebow where the locational information is aved in the Reference articulator. As the CM procedure, place both external acoustic meatus of the skull to the earplug portion of the virtual facebow in virtual dental space. By taking the anatomic structure such as orbit, dental midline, sagittal suture, spine as a reference, midline of the virtual facebow was adjusted. After that the





Figure 8. Digitized facebow for the virtual mounting technique. Scan the reference articulator and facebow complex, and place it to the Reference articulator file. The digitized facebow was aligned with the Reference articulator (Digitized facebow, Green).



orbitale pointer of the virtual facebow, the third reference point, was positioned at the same level as the right infraorbital notch of the skull (Figure 10B). This process is called **"Virtual facebow transfer"** that allows acquisition of the skull containing locational information mounted on a Reference articulator in STL format (Figure 10D). After completing this process, it can be confirmed that the condylar component of the articulator exists in the same position as the condylar head of the skull.

④ Position the Representative model fabricated in 2.3.2 to the skull file (Figure 10D). This process "Virtual mounting", and prepare data of virtual mounting technique by repeating the virtual facebow transfer and virtual mounting process five times for each subject (Figure 10).





Figure 9. The process for collecting the VM data. A. Convert DICOM files to the skull STL file. Both external acoustic meatus (yellow arrow) should be clearly expressed. B. Place the skull to the Digitized facebow. Place the earplug part of facebow on both acoustic meatus of the skull (red arrow), and the orbitale pointer of facebow at the same level as the right infraorbitale of skull (orange arrow). And finally, match the dental, facial midline to the center of facebow. C. The skull is located in the Reference articulator. D, E, F. The Representative model (pink) is superimposed on the skull. The following process is the same as for the CM.



2.2.4. Transfer to the coordinates system

Import the Representative models to reverse engineering software (Geomagic Control X, OR3D Ltd., Chirk, UK) to analyze Representative models placed via conventional mounting process (Figure 8F), and virtual mounting process (Figure 10H). Find coordinates of X, Y, Z-axis and the distance between coordinates on spatial coordinates by setting up the target points on the portion of teeth #11, 16, 26 (#11 mesial tip of incisal edge, #16 mesiobuccal cusp tip, #26 mesiobuccal cusp tip).

- Import the Representative models (Figure 8F,10H) that were repeatedly mounted (five times each for the same subject) to Geomagic Control X software (Figure 11A).
- (2) Target mesial tip of incisal edge of tooth #11, most prominent portion of mesiobuccal cusp tip of teeth #16, #26. The same target points can be set because all five models are dentical, although their locations are different (Figure 11B).
- ③ Identify the coordinates within the three-dimensional space of the five target points established in each tooth and measured the distance between the points. Since the distance will be measured in pairs, there should be a total of ten distance data per a tooth (Figure 11C, 12).
- Quantify the location information by applying the above process in teeth #11, 16, 26, and performing the CM as well as VM. The quantified coordinate values of the data were summarized in supplementary data (Supplementary table 1, 2).





Figure 10. Selection of the target points. A. 5 identical representative models. B. Set the target points at #11, 16, 26. Since all five models are identical, the same target point with only different locational information can be selected. C. Calculate the distance between target points.




Figure 11. Finding coordinates of the target points and distance between the target points via Geomagic control X software.



2.3. Data analysis

The data was analyzed in four ways. Firstly, the average distance between the five target points in the same tooth was estimated. Secondly, the standard deviation of X, Y, and Z coordinate of the same tooth was estimated. Thirdly, the significant difference analysis was performed for each coordinate value according to the order of trials at the target point of tooth #11. Lastly, the angle of the occlusal plane measured by linking the target point of the incisal edge of tooth #11 to the target point of the mesiobuccal cusp of tooth #16 was estimated.

2.3.1. Average distance between target points

The five target points selected in one tooth were paired up to obtain ten distance data by combination formula, and the average value was considered as the representative value. In 15 subjects, the average distance between target points for each tooth of each technique was calculated and summarized in Supplementary table 3.

2.3.2. Standard deviation of target points

The standard deviation was obtained for the X, Y and Z coordinates of the five target points for the each tooth and the results were summarized as Supplementary table 4, 5, 6.



2.3.3. Spatial relationship between each technique

The difference between the X, Y, Z coordinates for the order of repetitions in tooth #11 was analyzed. Since the purpose was to identify the tendency of coordinates for each technique, significant differences between the order of trials was examined. Then, the coordinates value itself was used to analyze the two data according to the order in which the mounting was performed with each technique (Supplementary table 7). In other words, the difference between the X, Y, Z coordinates of the first CM and VM conducted in 15 subjects were analyzed, followed by an analysis of the coordinates between the second mounting models. The analysis took place a total of five times for each coordinate values because the analysis was performed five times per a subject.

2.3.4. Average angle of the occlusal plane

According to GPT-9, occlusal plane is defined as "The average plane established by the incisal and occlusal surfaces of the teeth. Generally, it is not a plane but represents the planar mean of the curvature of these surfaces³." In this study, when measuring the angle of the occlusal plane, only two variables including the incisal edge of tooth #11 and the mesiobuccal cusp tip of tooth #16 were used as in the cephalometric analysis to minimize errors caused by variables in the analysis^{37, 38}. As shown in Figure 13, X-axis illustrates the lateral movements of the model. If the model moves to the right, the X coordinate value increases to the positive value, and if the model moves to the left, the X coordinate





Figure 12. Mounted models in coordinate system. To find the angle of the occlusal plane, orthogonal projection was made on the YZ plane.

value increases to the negative value. Y-axis expresses the forward and backward movement of the model. If the model moves forward, the Y coordinate value increases to the positive value, and if the model moves backward, the Y coordinate value increases to the negative value. Z-axis expresses the upward and downward movement of the model. If the model moves upward, the Z coordinate value increases to the positive value, and if



the model moves downward, the Z coordinate value increases to the negative value.

In this study, to find the angle of the occlusal plane, orthogonal projection of the target points of tooth #11 (mesial tip of incisal edge) and #16 (mesiobuccal cusp tip) on the YZ plane was obtained, and then the slope $(\Delta z/\Delta y)$ created by the two points was calculated. Arctangent ($\theta = \tan^{-1}x$) was calculated to this value and the angle of a line formed by two points was obtained in radian. Finally, the angle that the occlusal plane forms with the Yaxis was attained by converting the value into degrees (Supplementary table 8). The angle formed by the horizontal plane of the reference articulator and Y-axis on virtual dental space was also considered. Dispersed five dots were marked on the top of Reference articulator, which denotes the horizontal reference plane, orthogonal projection of those dots were obtained on the YZ plane. The five dots were paired up to make ten pairs using combination formula and the slope of a line formed by the two dots was obtained. The mean value of the slope (degrees) was added (Supplementary table 9) to the angle formed by the occlusal plane and the Y-axis to obtain the angle of the occlusal plane against the horizontal plane (Angle of the occlusal plane). The slope is expressed as a negative value when the posterior part is facing upwards than the anterior part. For the convenience in interpreting the data, -1 was multiplied to all data to change their sign. Because each technique was repeated five times per subject, the average of the angle of the occlusal plane measured five times was used as a representative value for statistical analysis.



2.4. Statistical analysis

A statistical software (SPSS v23.0, SPSS Inc, IL, USA) was used for comparative analysis of the two groups, CM and VM. The level of significance for all statistical analyses was set to be 0.05.

2.4.1. Average distance between target points

A statistical analysis was performed by setting the average of 10 distance data per tooth obtained through a combination formula in 15 subjects as representative values. The Kolmogorov-Smirnov test was performed to evaluate the normality of data. All of the data did not follow the normal distribution, the Wilcoxon signed-rank test was used to perform comparative analysis for CM and VM.

2.4.2. Standard deviation of target points

A statistical analysis was conducted for the standard deviation obtained from 15 subjects according to teeth and coordination. Kolmogorov-Smirnov test was performed to evaluate normality of data. Since X coordination in tooth #16 in the VM did not follow the normal distribution, Wilcoxon signed-rank test was performed exceptionally for X-axis of tooth #16, and paired t-test for the rest.



2.4.3. Spatial relationship between each technique

One-way RM-ANOVA was performed on each of the coordinates to find out whether there is a significant difference depending on the order of trials in tooth #11. Then, the difference between the X, Y, and Z coordinates of the CM and VM for the same number of trials was analyzed. The purpose was to identify the tendency of coordinates for each technique, therefore, instead of setting representative value, naïve data was used, and the two data was analyzed by mounting sequence. Kolmogorov-Smirnov test was performed to evaluate the normality of data. Wilcoxon signed-rank test was performed for Z coordinate of the second trial, X and Y coordinates of the third trial, X coordinates of the fourth trial, Y coordinates of the fifth trial that did not follow normality. A paired t-test was conducted for the rest of the data that followed normality.

2.4.4. Average angle of the occlusal plane

A statistical analysis was performed by setting the average value of the angle of the occlusal plane measured five times per person in 15 subjects as representative value. According to the result of the Kolmogorov-Smirnov test, both the CM and VM followed the normality. Therefore, paired t-test was conducted.



3. RESULT

The result of CM and VM are as follows (Figure 14).

| | Conventional mounting | Virtual mounting | C+V (Occlusal) | C+V (Rt.) | C+V (Lt.) |
|--------------|--------------------------|---------------------|-------------------|--------------|--------------|
| Subject 1 | | | | | lippac |
| Subject 2 | | | | | |
| Subject 3 | | | | | Marine . |
| Subject 4 | | | | Sure Con | 111111 |
| Subject 5 | | | | | Dennau fal |
| Subject 6 | | | | - | |
| Subject 7 | | | R | | Intrast |



| | Conventional mounting | Virtual mounting | C+V (Occlusal) | C+V (Rt.) | C+V (Lt.) |
|---------------|--------------------------|---------------------|-------------------|---------------------------------------|-----------------------------------------------------------------------------------------------------------------|
| Subject 8 | | | | | (Dalance) |
| Subject 9 | | | | (Jacob) | WELLER |
| Subject 10 | | | | A A A A A A A A A A A A A A A A A A A | 10-A-T |
| Subject 11 | | | | | |
| Subject 12 | | | | | BALLY |
| Subject 13 | | | | | in the second |
| Subject 14 | | | | | |
| Subject 15 | | | R | And State | |

C: conventional mounting, V: virtual mounting

Figure 14. Positional relationships between mounted models with CM and VM



3.1. Average distance between target points

The mean distance between the two points measured in teeth #11, 16, and 26 was smaller in VM than CM, and these values were statistically significantly different between the two techniques in all the teeth #11, 16 and 26 (Table 2). Besides, the displacement between the maximum and minimum values was more in the CM than the VM (Figure 15). Suppose the mounting is repeated with each technique; the distance between the target points is closer in the VM than that of the CM, which signifies that the target points are present within the smaller radius. That is, the VM may have higher precision than the CM. The degree of errors that occurred in each mounting technique is shown in Figure 14. All the mounting cases performed using the CM had more errors within the group compared with the mounting cases performed with the VM. Among subjects in the CM, subject number 4 and 12 particularly showed more errors. In the case of subject number 9 and 13, the degree of error between the two techniques was comparable.

The Bland-Altman plot shows the range of deviations of the average distance of the target point in both CM and VM^{39, 40} (Figure 16). The mean value of difference between average distance of teeth #11, 16, 26 are 2.58, 2.81, 2.77, respectively, and the data of the CM does not correspond with the data of the VM. The mean distance of the CM tends to be systemically larger than that of VM. Also, all three data showed an ascending diagonal graph, which signifies that there is a strong correlation between the mean value and measured difference value.



| | Mean ± SD | | |
|-----|-----------------------|------------------------|--|
| | Conventional mounting | Virtual mounting | |
| #11 | 4.7239 ± 1.4461 | 2.1401 ± 0.5813 | |
| #16 | 5.1653 ± 1.5397 | 2.3521 ± 0.6044 | |
| #26 | 4.9636 ± 1.5543 | 2.1887 ± 0.5484 | |
| | | SD, standard deviation | |

Table 2. Precision of the each technique (Average distance)



Figure 13. Box-plot table for the average distance of the target points. Comparison among groups is expressed as **P < 0.01, asterisks and horizontal bars indicate statistically significant differences among groups.





Figure 14. Bland-Altman plot for the average distance. SD, standard deviation



3.2. Standard deviation of target points

The standard deviation between the target points specified in teeth #11, 16, 26 showed greater values for the case of CM than the VM, all values showed statistically significant differences (Table 3, Figure 17). When each technique was repeated, each target point was more densely located for VM, implying that fewer spatial errors occur with the VM. In other words, along with the results of experiment number 1 (Average distance), it can be concluded that the VM has higher precision than the CM. In addition, while VM did not show tendency according to X, Y, Z-axis, the CM showed a huge displacement between the maximum and minimum values of the Z-axis standard deviation (Figure 17). This means that CM lacks upward and downward repeatability than anteroposterior and lateral errors.

Table 3. Precision of each technique (Standard deviation)

| | | Mean ± SD | | |
|-----|--------------|---------------------|---------------------|---------------------|
| | | SD of X Coordinate | SD of Y coordinate | SD of Z coordinate |
| #11 | Conventional | 1.5951 ± 0.6368 | 2.1568 ± 0.7458 | 2.0562 ± 1.3497 |
| | Virtual | 1.0690 ± 0.4705 | 0.7952 ± 0.2868 | 0.8021 ± 0.2695 |
| #16 | Conventional | 1.8095 ± 0.6770 | 2.3042 ± 0.8684 | 2.1641 ± 1.6198 |
| | Virtual | 1.1170 ± 0.4517 | 0.9923 ± 0.3956 | 0.8085 ± 0.2760 |
| #26 | Conventional | 1.8227 ± 0.7086 | 2.0559 ± 0.0815 | 2.1984 ± 1.5970 |
| | Virtual | 1.1225 ± 0.4536 | 0.8434 ± 0.3283 | 0.7420 ± 0.2275 |

SD, standard deviation





Figure 17. Box-plot table for the standard deviation. Comparison among groups is expressed as *P < 0.05, **P < 0.01, ***P < 0.001, asterisks and horizontal bars indicate statistically significant differences among groups. C, conventional mounting; V, virtual mounting

Bland-Altman plot depicts the range of deviations of the standard deviation of X, Y, Zaxis of the CM and VM (Figure 18-20). Since all X, Y, Z-axis of teeth #11, 16, 26 have positive mean values, the standard deviation of the CM is systemically big, and the data between the two groups does not coincide. However, the difference between the two measurements show a specific tendency to increase in a positive direction.





Figure 15. Bland-Altman plot for the standard deviation of #11. SD, standard deviation





Figure 16. Bland-Altman plot for the standard deviation of #16. SD, standard deviation





Figure 17. Bland-Altman plot for the standard deviation of #26. SD, standard deviation



3.3. Spatial relationship between each technique

For both CM and VM, there was no significant difference by the order of repetitions (Figure 21). That is, repeating both techniques five times in a subject did not result in an increase or decrease of errors. Subsequently, a significant difference between each coordinate by order of repetitions in both the CM and VM was examined (Figure 22). In the case of the X coordinate, there was no significant difference between the CM and VM from the first to the fifth repetition. On the other hand, Y coordinate showed a significant difference in a positive direction in the case of VM from the first up to the fifth repetition. This finding can be interpreted that the dental cast is more anteriorly located in VM than CM. The results are shown in Figure 14. From the model's occlusal view, all 15 data are located ahead of CM in the case of VM. In the case of the Z coordinate, the coordinates of the CM were higher than the VM in the fifth repetitions only. In other words, in one out of the five-repeated experiments (20%), the cast is located more upwards in the CM compared with the VM.





X-axis of the graph, the order of repetitions; Y-axis of the graph, the coordinate value corresponding to X-axis

Figure 18. Result of one-way RM-ANOVA to analyze the significant difference between trials. There was no significant difference according to the order of trials in both the CM and VM.





Figure 19. Box-plot table for the analysis of coordinate values according to the order of trials. Comparison among groups is expressed as *P < 0.05, **P < 0.01, ***P < 0.001, asterisks and horizontal bars indicate statistically significant differences among groups. C, conventional mounting technique; V, virtual mounting technique; X, Y, Z means each coordinates; the number of X-axis means the order of trials.



3.4. Average angle of the occlusal plane

The mean angle of the occlusal plane measured by the CM was 8.14°, whereas it was 2.13° measured by the VM. The angle of the occlusal plane was statistically significantly steeper in the CM compared with that of the VM. Similarly, the maximum value for each group was greater in the CM compared to VM (Table 4, Figure 23).

Table 4. Precision of each technique (Angle of the occlusal plane)

| | Mean \pm SD | Maximum value |
|--------------|---------------------|---------------|
| θc (degrees) | 8.1383±7.8334 | 19.4249 |
| θv (degrees) | 2.1280 ± 7.5637 | 14.4137 |

 θ , angle of the occlusal plane; c, conventional technique; v, virtual technique





Figure 20. Box-plot table for the angle of the occlusal plane. Comparison among groups is expressed as ***P < 0.001, asterisks and horizontal bars indicate statistically significant differences among groups. θ , angle of occlusal plane; c, conventional mounting technique; v, virtual mounting technique.

Except for the subject number 6, all the mean angle of CM (θ c) values were greater than mean angle of VM (θ v), and subject number 6 also showed a minimum angle difference of less than 1 degree between the CM and VM. In the case of the subject numbers 3, 8, and 12, the angle formed by the occlusal plane and the horizontal plane was shown to be a



negative value, but mean θ c tended to be greater than mean θ v. For the subject number 10, 11, and 15, the angle of the occlusal plane was shown to be positive for the CM, and negative for the VM. However, the tendency of the posterior part of the cast mounted with the CM being located upwards compared to the VM remained the same. This tendency is illustrated in Figure 14. As shown in the two columns on right displaying both CM and VM model, while there were individual differences by degree and quantity, the tendency of the occlusal plane heading downward for VM remained the same.

Bland-Altman plot depicts the range of deviation of the angle of the occlusal plane (Figure 24). Since Y-axis shows positive values in all except for one data, the angle of the occlusal plane measured by the CM is generally greater than the measured value of the VM; and the mean value was 6.05, showing a big difference between the two groups. Also, the upper limits of agreement (LOA) was 14.35, lower LOA was -2.24, and the 95% difference between the two techniques was 16.59° that fell within the range of big difference.





θ, Angle of occlusal plane; c, conventional mounting technique; v, virtual mounting technique

Figure 21. Bland-Altman plot for the angle of the occlusal plane. Since Y-axis shows positive values in all except for one data, the angle of the occlusal plane measured by CM is generally greater than VM.



4. DISCUSSION

The introduction of digital technology in dentistry has led to the shifting of conventional methods to digital techniques. However, problems often occur while placing a digitized dental model to a virtual articulator. Since the indirect digital method is complicated and has complex procedures, several techniques were suggested to overcome this problem, yet no definite methods have been adopted so far.

Therefore, this study presents the CBCT based direct digital facebow transfer procedure. A comparative analysis was performed between CM and VM on the four aspects: the average distance between the target points, the standard deviation of target points for each axis, the positional relationship between each technique for the X, Y, Z-axis of tooth #11, and the angle of the occlusal plane (Figure 2). By the result, the null hypothesis of this study, there is no difference between the CBCT based VM and an anatomic facebow based CM is rejected. Also, it is confirmed that the VM has higher precision than the CM.

According to the International Organization for Standardization (ISO 5725-1), accuracy consists of trueness and precision. Trueness measures the closeness of agreement between the arithmetic mean and the true value, and precision measures the closeness of agreement between test results. The trueness was not measured, because this study was conducted on human body measuring the true values. Other in vivo study also measured the precision and not the trueness because they could not set the true value⁴¹. Another study insisted that their findings were "trueness", but in fact, they were measuring the spatial deviation



between the two measurements¹⁸. Thus, additional studies are required to investigate the method of setting the true value for in vivo study.

When the FOV of CBCT is large, the accuracy is lower than that of the small FOV because the beam angulation becomes more severe in the superior and inferior volume areas and the contrast to noise ratio decreses⁴². Since the voxel size in the P mode of the CBCT used in this study had a specific voxel size (0.3/voxel (mm)), not adjustable, so it is difficult to assess the influence of this variable. The voxel size of CBCT has a great influence on the noise of the orthogonal slices. If the voxel size is small, the noise increases, but the spatial resolution is better⁴³. In this study, the image was taken in P mode, which can reproduce all the anatomical structures necessary for the VM without violationg the ALARA principle. But the additional study will be needed to understand the relationship between all parameters related to the radiation dose and the accuracy of the reconstructed image during CBCT imaging.

Moreover, this study included a minimum number of subjects to prevent unnecessary exposure of subjects to radiation due to the CBCT procedure. Consequently, race, sex, age, craniomandibular relation, etc., were not considered.. Since the study recruited subjects with the least number of restorations, no missing teeth and TMJ disorder, the age of the subjects included in this study were mostly in their 20s to 30s.



4.1. Average distance between target points

In an experiment that measured the difference in the mean distance among the target points between the CM and VM, the difference was significantly more in the CM compared to the VM. That is, even if one operator repeats the procedure five times without a pause, the error occurs more in the CM. The subject's strong resistance to facebow transfer procedure can affect the repeatability of the procedure. Especially, earplug insertion causes discomfort to the subject, which makes it difficult to place the facebow at correct position. On the other hand, the operator can manipulate the facebow as she intended in the VM, thereby produce fewer errors than the CM. Besides, in circumstances where both porions are not parallel due to facial asymmetry, or dental midline and facial midline does not coincide, errors are invisible with the naked eye if facebow transfer is directly performed to the patient. However, minute differences can be perceived when manipulating the skull on virtual dental space. Errors can be minimized even if facial midline and dental midline does not coincide, because there are still several anatomic points that can be used as references such as vomer bone, sagittal suture, spine, etc. The earplug and orbitale pointer, which determines the lateral and horizontal factors, are located on soft tissues. But in the skull, anatomic reference point is constant, so there will be fewer errors. Nevertheless, the initial orientation of external acoustic meatus is not parallel with the horizontal axis, and it can be affected by the subject's skull size and CBCT's field of view during the CBCT imaging process. In other words, if the size of the subject's skull is too big, it should be



noted that it is the pathway of the external acoustic meatus that is reproduced on the skull and not the porions.

4.2. Standard deviation of target points

In the standard deviation measured by coordinates to determine the distribution of target points according to X, Y, Z-axes showed more compact target points of VM in all cases. Along with the results of test number 1 (Average distance), this results indicate that the VM has higher precision than the CM. In Figure 17, Z-axis of the CM showed big difference between the maximum and minimum standard deviation compared with other axes. Additionally, hardening expansion of dental plaster used in CM may have contributed to this difference as well. Despite the right mixing ratio and setting time, hardening expansion is affected by the surrounding environment such as moist and temperature. Cast mounting was carried out in a designated place. However, the weather, temperature, and surrounding environment at the time of mounting forms the factors of error.

4.3. Spatial relationship between each technique

There were no significant differences according to repeated trials in the X, Y, and Z-axes for the CM and VM in tooth #11. That is, repeating the mounting in a same subject does not increase or reduce errors. In a comparative analysis of the coordinates of each technique



by the order of trials to pair up the CM and VM, the findings showed that the VM was always positioned ahead of the CM. This is because there was a positional difference between the porion of CBCT and that of soft tissue where the earplug of the facebow was inserted. There was a difference in degree for each subject, the porion on the CBCT located more posteriorly and upwardly than the porion on the soft tissue (Figure 25). If the porion on CBCT is located more posteriorly than the porion on soft tissue, the cast of VM is located more anteriorly.



Figure 22. Positional difference of the porion on soft tissue and skull. The porion of the skull is located more posteriorly and upwardly to the porion of the soft tissue.



The external acoustic meatus is a gentle S-shaped 2.5cm long canal consisting of two parts, i.e., inner two third bony part, and the outer one third cartilaginous part. When the canal is looked at from the horizontal view, the external part is protruded forward, and the inner part is protruded backward⁴⁴. Due to the limitation of the CBCT's FOV, the external auditory canal is cut in external part on skull of VM, the effect of pathway of the auditory canal seems to be insignificant.

In actual clinical practice, the position of the anterior teeth when mounting on the articulator determines the anterior guidance and is determining the cusp height and cusp angle of the posterior teeth^{45, 46}. Since it was impossible to set the true value for measuring the trueness of each technique, it would be a good attempt to try both techniques in making a simple prosthesis for patient.

In Z-axis, the coordinates of the CM were located significantly higher than that of the VM in the fifth trial (20%). Here, factors such as discomfort from earplug insertion and plaster expansion during gypsum mounting must have affected the result. However, such a trend appeared only in one out of five trials, and thus considered insignificant.

4.4. Angle of the occlusal plane

The angle of the occlusal plane measured by the CM was statistically steeper than that of the VM. The average value of angle of the occlusal plane in the case of the CM was $8.13834\pm7.8334^{\circ}$, and $2.1280\pm7.5637^{\circ}$ for VM, which was within the range of $1-9^{\circ 37, 47, 48}$,



the adult mean value for Frankfort horizontal plane determined by previous studies. But both techniques seem to differ from previous study when considering the standard deviation of 7° or more. The mean angle of occlusal plane measured in 60 Koreans in another study was $9.75 \pm 3.41^{\circ 49}$, and showed a difference with our study, too. In that study, there was no significant difference between angles of the occlusal plane when they compared the left to right. Also, they found no significant gender difference. Therefore, this study considered the characteristics of the subject as a factor of an error. The occlusal plane is affected by the skeletal class of the subject. However, the skeletal class of the 15 subjects was not considered, and 7 out of 15 subjects even had an orthodontic treatment history. Because the angle of the occlusal plane has individual variations, the number of subjects recruited for this study was too small to draw a specific conclusion with the result obtained from this study..

The angle of the occlusal plane for CM was stiffer than the VM. This can be explained by the difference in position of porion on soft tissue and skull as result of experiment 3 (Figure 25). Since the porion, the posterior reference point of facebow, is located more downward on the soft tissue, the angle of occlusal plane of the CM is stiffer.

A study that compared the angles of the occlusal plane between the CM and VM via Stereophotogrammetry²⁶ also showed a stiffer occlusal plane angle in CM. However, that study had set Frankfort horizontal plane as a horizontal reference plane during the CM, and Natural head position (NHP) as a horizontal reference plane during the VM. Consequently, differences in angles between those horizontal reference planes can also occur, and it is



uncertain to take such a finding as a reference.

This study presents a CBCT based VM performed on virtual dental space, and the CM using an anatomic facebow. Also, it conducted a comparative analysis of the difference between the locational relationships of the two techniques and evaluated the repeatability of each technique. The VM showed higher precision in the aspect of average distance and standard deviation between the target points compared with the CM. Also, in tooth #11, definitive cast situated ahead of the CM.

According to previous study, the true hinge axis exists in the lower part of the condyle⁵⁰. To compare the condylar position in both techniques, the skull was superimposed on the CM model (Figure 26). As a result, the condylar component of the articulator and the condyle of the skull after mounting were consistent with both the VM and the CM, and the VM tend to be positioned more downward than CM. In order to determine which of the two technique has higher trueness, an additional study is needed to compare and analyze the two techniques in actual clinical practice.

In the process of superimposing CBCT and dental cast, it is difficult to apply the VM suggested in this study for patients with multiple missing teeth or edentulous patients. Further research is required for these cases. In dentulous patients, the CBCT based VM can be used as an excellent tool to establish total digital dentistry with JMA system using ultrasound impulse to reproduce mandibular movements or jaw tracking system using optic technology.





Figure 23. Condylar component of the articulator and condylar location of the CM and VM. Blue, skull of CM; Green, skull of VM



5. CONCLUSION

- 1. The VM shows higher precision in the aspect of average distance between the coordinates than the CM.
- 2. The VM shows higher precision in the aspect of standard deviation between the coordinates than the CM.
- For the VM, there was not much difference in the degree of error in the X, Y, Z-axis direction between each trial. Whereas in the CM, the error in the Z-axis direction, i.e., the error in the upward and downward, was the largest.
- The cast mounted with the VM positioned ahead of the cast mounted with the CM.
 Also, CM cast tends to be positioned higher than the cast of the VM (20%).
- 5. When the cast is mounted with CM, the angle of the occlusal plane tended to be steeper than that of VM.



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SUPPLEMENTARY DATA

Supplementary table 1. Naïve data - coordinates of conventional mounting

| Subject Order of | | | #11 | | | #16 | | | #26 | | |
|------------------|-------------|---------|---------|----------|---------|----------|----------|----------|----------|----------|--|
| No. | Repetitions | х | У | Z | Х | У | Z | Х | У | Z | |
| | 1 | 1.7104 | 1.34 | 585.2681 | 20.2684 | -22.1807 | 589.8628 | -17.0479 | -19.1161 | 590.5655 | |
| | 2 | 2.9852 | 2.2881 | 584.1472 | 21.802 | -20.895 | 589.4702 | -15.3881 | -18.5254 | 588.1935 | |
| 1 | 3 | 2.8432 | -0.7462 | 584.4546 | 20.7751 | -24.5127 | 590.5597 | -16.4404 | -20.6268 | 589.2072 | |
| | 4 | -2.9666 | 2.1246 | 586.3671 | 15.3353 | -21.4031 | 592.2965 | -21.8934 | -17.9546 | 591.311 | |
| | 5 | 0.0667 | 3.4499 | 586.5818 | 18.9616 | -19.6747 | 592.0104 | -18.3056 | -17.3901 | 590.5109 | |
| | 1 | 1.527 | 10.7433 | 579.2816 | 20.6051 | -21.675 | 588.2198 | -20.3338 | -21.5014 | 586.7239 | |
| | 2 | 4.8214 | 13.4005 | 578.1086 | 24.264 | -18.7273 | 587.0594 | -16.6012 | -19.4107 | 584.0547 | |
| 2 | 3 | 1.0247 | 8.3787 | 579.535 | 20.9131 | -23.7224 | 588.3372 | -19.9838 | -24.5046 | 586.2573 | |
| | 4 | 1.7764 | 8.3393 | 579.8455 | 21.3393 | -23.7822 | 589.3235 | -19.5684 | -24.0381 | 588.3625 | |
| | 5 | 1.3616 | 7.9297 | 579.9649 | 20.5693 | -24.5622 | 588.3025 | -20.3981 | -24.2243 | 587.6122 | |
| | 1 | 6.1582 | 4.9126 | 591.2545 | 23.0331 | -20.7375 | 589.547 | -22.5572 | -17.6235 | 588.0381 | |
| | 2 | 4.6815 | 9.3873 | 594.5491 | 23.149 | -14.8935 | 590.8669 | -22.6198 | -14.7253 | 590.9231 | |
| 3 | 3 | 8.1705 | 10.3241 | 594.0894 | 26.2575 | -14.2789 | 591.0394 | -19.5412 | -13.366 | 590.3058 | |
| | 4 | 4.7233 | 7.2603 | 590.0572 | 22.4804 | -17.5347 | 588.1362 | -23.1586 | -16.4125 | 587.5294 | |
| | 5 | 5.2143 | 12.1193 | 589.438 | 23.3188 | -12.2937 | 586.7906 | -22.4307 | -11.574 | 586.1705 | |
| | 1 | 5.8202 | 15.3797 | 591.6124 | 24.3742 | -14.5915 | 598.0585 | -19.9126 | -17.7615 | 597.9047 | |
| | 2 | 6.47 | 11.6125 | 593.7813 | 26.3545 | -17.9991 | 597.2184 | -17.8818 | -23.0842 | 596.9295 | |
| 4 | 3 | 5.9061 | 9.9658 | 594.188 | 26.0248 | -19.457 | 597.3773 | -18.1008 | -24.731 | 597.56 | |
| | 4 | 5.1423 | 13.6079 | 592.065 | 24.3746 | -16.174 | 597.6584 | -20.0681 | -20.0235 | 597.9598 | |
| | 5 | 1.1065 | 9.0712 | 593.2595 | 19.8938 | -21.0296 | 597.3513 | -24.4299 | -24.4629 | 597.3851 | |
| | 1 | 3.4836 | 9.2698 | 586.312 | 24.9703 | -18.9446 | 593.1911 | -21.3381 | -18.8967 | 590.9265 | |



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| | 2 | 7.5079 | 5.934 | 587.7987 | 29.5473 | -21.6208 | 595.2148 | -16.7232 | -22.5839 | 592.9017 |
|----|---|--------|---------|----------|---------|----------|----------|----------|----------|----------|
| F | 3 | 6.4996 | 11.2731 | 581.6717 | 28.7765 | -16.4832 | 588.1838 | -17.5436 | -17.396 | 587.6584 |
| C | 4 | 5.3056 | 7.2111 | 585.1056 | 27.1563 | -20.6388 | 591.9766 | -18.9258 | -21.2832 | 589.6375 |
| | 5 | 7.1131 | 11.0214 | 582.9213 | 29.0592 | -16.7762 | 589.8831 | -17.1892 | -17.4743 | 588.3542 |
| | 1 | 6.6678 | 10.1602 | 586.442 | 27.0235 | -16.5453 | 592.0376 | -21.8952 | -14.143 | 590.6306 |
| | 2 | 6.054 | 9.1981 | 584.8027 | 25.9293 | -17.5746 | 590.9606 | -23.0017 | -14.7498 | 588.877 |
| 6 | 3 | 7.5587 | 8.1592 | 584.9859 | 27.5637 | -18.4773 | 591.3123 | -21.3222 | -15.8166 | 589.3813 |
| | 4 | 6.788 | 10.4731 | 585.7979 | 27.4547 | -15.433 | 592.8502 | -21.4127 | -14.3772 | 590.51 |
| | 5 | 4.8776 | 12.7148 | 584.9714 | 25.5245 | -13.7291 | 589.9465 | -23.4503 | -12.0932 | 589.3718 |
| | 1 | 5.686 | 12.3615 | 587.6111 | 29.0575 | -15.5641 | 591.8115 | -23.6314 | -17.022 | 587.897 |
| | 2 | 6.4459 | 17.8886 | 590.7034 | 29.3365 | -10.5488 | 593.5077 | -23.3526 | -10.9769 | 589.3588 |
| 7 | 3 | 6.1201 | 14.9791 | 592.0922 | 30.4781 | -12.022 | 596.6113 | -22.2665 | -15.2794 | 594.1757 |
| | 4 | 7.2642 | 14.904 | 593.5647 | 29.6178 | -14.0833 | 596.9197 | -23.2844 | -13.3343 | 594.6607 |
| | 5 | 5.406 | 14.9696 | 591.44 | 27.7685 | -13.3578 | 597.4974 | -24.993 | -13.5122 | 593.6773 |
| | 1 | 4.4131 | 12.9498 | 586.9499 | 24.3847 | -15.8783 | 582.9653 | -21.8453 | -19.8687 | 582.0854 |
| | 2 | 4.2609 | 11.4545 | 585.9567 | 24.2898 | -17.5834 | 584.4594 | -21.8923 | -21.5159 | 580.8391 |
| 8 | 3 | 4.1975 | 7.6167 | 587.3652 | 21.4833 | -22.9681 | 583.6647 | -24.9841 | -22.5915 | 582.5349 |
| | 4 | 5.3446 | 12.1158 | 584.9882 | 25.736 | -16.6048 | 582.239 | -20.6632 | -21.0888 | 580.9869 |
| | 5 | 5.5936 | 7.6851 | 583.1362 | 24.8027 | -21.82 | 581.3737 | -21.6974 | -24.724 | 581.7274 |
| | 1 | 6.1753 | 10.0438 | 591.059 | 25.4641 | -11.7935 | 596.027 | -23.7565 | -15.0768 | 591.695 |
| | 2 | 6.6893 | 11.7122 | 590.3781 | 26.4262 | -9.5923 | 595.7223 | -22.7003 | -13.852 | 592.4411 |
| 9 | 3 | 6.4316 | 12.0183 | 588.269 | 27.0493 | -9.1116 | 590.5222 | -22.1931 | -14.3539 | 590.8066 |
| | 4 | 6.5889 | 9.1489 | 587.0955 | 26.3431 | -12.3021 | 591.6585 | -22.7546 | -16.6578 | 587.4806 |
| | 5 | 9.2333 | 10.9474 | 586.5624 | 28.5514 | -11.2262 | 589.7493 | -20.771 | -13.931 | 586.2343 |
| | 1 | 7.9874 | -5.9247 | 584.3834 | 25.3906 | -21.6453 | 583.811 | -13.6669 | -24.3817 | 583.4937 |
| | 2 | 1.895 | -5.7358 | 589.8515 | 18.9272 | -21.6016 | 590.6978 | -20.0147 | -23.8445 | 588.5161 |
| 10 | 3 | 3.0475 | -4.2998 | 587.8209 | 21.9324 | -20.5686 | 592.3745 | -18.5027 | -22.7955 | 587.7844 |
| | 4 | 5.1131 | -1.7199 | 589.99 | 20.4866 | -20.037 | 587.8973 | -16.8709 | -19.7122 | 589.5984 |



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| | 5 | 4.1242 | -5.508 | 591.7745 | 22.1921 | -17.7049 | 591.2438 | -17.0125 | -24.5275 | 591.3124 |
|----|---|---------|---------|----------|---------|----------|----------|----------|----------|----------|
| | 1 | 4.0703 | 6.657 | 592.9933 | 27.8962 | -17.5681 | 593.1816 | -24.6755 | -23.9959 | 591.2065 |
| | 2 | 7.855 | 6.7308 | 593.0864 | 31.9386 | -17.0508 | 591.8939 | -20.5299 | -24.2075 | 591.0601 |
| 11 | 3 | 5.2415 | 8.1975 | 591.9824 | 29.4233 | -15.4979 | 592.8591 | -23.0021 | -22.9354 | 591.8055 |
| | 4 | 1.1907 | 8.5265 | 592.7513 | 23.9779 | -16.5585 | 592.2623 | -28.7989 | -20.78 | 590.6041 |
| | 5 | 5.806 | 11.842 | 591.3746 | 30.3867 | -11.6176 | 591.3676 | -22.0672 | -19.6234 | 591.3971 |
| | 1 | 5.7459 | -3.3492 | 590.647 | 23.6004 | -21.7671 | 588.5982 | -22.6669 | -18.8253 | 588.2768 |
| | 2 | 4.7565 | 6.3646 | 585.0916 | 23.6027 | -11.2689 | 585.3027 | -22.7084 | -10.59 | 582.1874 |
| 12 | 3 | 5.0075 | -3.7218 | 589.0207 | 22.8953 | -22.2699 | 589.3446 | -23.2755 | -19.343 | 587.1899 |
| | 4 | 6.1279 | 1.292 | 587.2994 | 24.4483 | -16.9314 | 587.7795 | -21.8003 | -14.7147 | 584.5009 |
| | 5 | 0.3302 | -0.9513 | 590.3802 | 18.9537 | -18.932 | 590.1117 | -27.4305 | -17.5615 | 588.8005 |
| | 1 | 10.4638 | 5.2973 | 580.0813 | 25.0905 | -25.8569 | 586.4413 | -16.9928 | -27.2576 | 589.4273 |
| | 2 | 5.8148 | 4.6681 | 596.5938 | 20.247 | -26.3668 | 603.8687 | -21.7855 | -27.6882 | 606.1904 |
| 13 | 3 | 10.6122 | 7.2212 | 589.9442 | 26.1357 | -23.2163 | 597.4916 | -15.8271 | -26.0321 | 599.7418 |
| | 4 | 11.0165 | 3.931 | 589.1316 | 27.2799 | -26.0207 | 597.1762 | -14.5616 | -29.2481 | 601.2838 |
| | 5 | 9.9069 | 4.373 | 590.2405 | 25.8311 | -25.5475 | 598.9362 | -16.0989 | -29.0294 | 600.7643 |
| | 1 | 4.0403 | 12.1093 | 594.1094 | 27.4654 | -11.589 | 602.0187 | -20.8133 | -10.2569 | 592.3279 |
| | 2 | 7.1714 | 11.3195 | 596.1979 | 30.8092 | -11.4056 | 606.0938 | -17.7073 | -10.9327 | 597.5823 |
| 14 | 3 | 6.225 | 14.6841 | 588.7863 | 29.9236 | -8.9779 | 596.1238 | -18.4233 | -7.8737 | 586.7692 |
| | 4 | 5.9093 | 10.1864 | 589.7852 | 28.9692 | -14.2669 | 596.5927 | -19.3763 | -11.7179 | 587.4524 |
| | 5 | 6.8187 | 7.6155 | 588.755 | 29.8638 | -16.3593 | 597.0909 | -18.4526 | -14.2658 | 587.7283 |
| | 1 | 4.3357 | 4.0699 | 590.0557 | 22.3861 | -20.1816 | 593.3503 | -19.7382 | -23.4804 | 590.5156 |
| | 2 | 6.2255 | 5.2567 | 588.8212 | 23.9673 | -18.9797 | 592.81 | -18.251 | -21.7457 | 592.3304 |
| 15 | 3 | 4.2454 | 5.9503 | 592.3437 | 20.8631 | -19.341 | 594.3467 | -21.4188 | -20.1233 | 593.7775 |
| | 4 | 4.411 | 3.2017 | 591.2676 | 21.4557 | -21.5065 | 595.8773 | -20.7688 | -23.2836 | 594.258 |
| | 5 | 5.0148 | 7.5449 | 591.8329 | 22.2482 | -17.2938 | 594.2537 | -19.9392 | -19.2437 | 593,7995 |



| Subject | Order of | | #11 | | | #16 | | | #26 | |
|---------|-------------|--------|---------|----------|---------|----------|-----------|----------|----------|----------|
| No. | Repetitions | х | у | Z | Х | у | Z | Х | у | Z |
| | 1 | 2.8611 | 14.7741 | 587.9949 | 20.5663 | -9.1815 | 589.1989 | -16.6099 | -8.1608 | 588.4579 |
| | 2 | 1.165 | 16.1205 | 588.2723 | 18.726 | -7.9103 | 590.3941 | -18.4313 | -6.6131 | 589.3481 |
| 1 | 3 | 2.7115 | 13.8259 | 587.1978 | 19.9344 | -10.6113 | 589.0161. | -17.2483 | -8.6555 | 587.7126 |
| | 4 | 0.7437 | 15.2014 | 588.5252 | 18.9949 | -8.4184 | 590.9927 | -18.242 | -8.0785 | 589.8206 |
| | 5 | 1.9868 | 15.6604 | 588.1052 | 19.9882 | -8.3796 | 589.3938 | -17.2457 | -7.3245 | 588.613 |
| | 1 | 3.0286 | 15.568 | 576.266 | 22.3258 | -17.4665 | 581.2682 | -18.6448 | -17.2934 | 578.9493 |
| | 2 | 0.1446 | 16.5292 | 576.2157 | 19.445 | -16.4315 | 580.7159 | -21.5001 | -16.3703 | 578.8734 |
| 2 | 3 | 1.8779 | 16.1698 | 578.212 | 21.7843 | -16.4725 | 582.0548 | -19.0498 | -17.2443 | 580.1874 |
| | 4 | 2.0794 | 16.6715 | 576.0414 | 21.3392 | -16.2027 | 580.8032 | -19.4389 | -16.3224 | 579.8628 |
| | 5 | 1.8206 | 17.2813 | 577.0875 | 21.1323 | -15.8327 | 579.3741 | -19.5607 | -15.8992 | 577.8314 |
| | 1 | 6.4436 | 13.0757 | 588.3946 | 23.7693 | -11.9506 | 585.6844 | -21.9354 | -9.6319 | 584.8671 |
| | 2 | 8.2233 | 15.093 | 588.1695 | 25.5709 | -9.9547 | 585.0348 | -20.149 | -7.8632 | 584.3286 |
| 3 | 3 | 7.3819 | 13.4973 | 588.576 | 24.7488 | -11.7299 | 585.22 | -21.0037 | -9.2511 | 584.1521 |
| | 4 | 7.0884 | 12.623 | 586.5795 | 24.9283 | -12.1049 | 583.6241 | -20.8096 | -11.0062 | 582.9564 |
| | 5 | 6.3297 | 13.4825 | 589.0939 | 24.1251 | -11.4522 | 585.9924 | -21.5176 | -9.8987 | 584.7305 |
| | 1 | 7.9869 | 16.9227 | 586.0261 | 27.2613 | -13.0376 | 588.0121 | -17.0439 | -17.1891 | 587.4221 |
| | 2 | 7.2988 | 17.3815 | 587.402 | 25.1779 | -13.5516 | 588.5295 | -19.2753 | -15.5863 | 587.9793 |
| 4 | 3 | 5.7679 | 15.9663 | 586.9348 | 23.7569 | -14.8456 | 588.2874 | -20.6494 | -17.013 | 588.4296 |
| | 4 | 7.9587 | 15.9641 | 585.8848 | 26.8859 | -14.4388 | 586.5228 | -17.4346 | -17.9143 | 586.36 |
| | 5 | 4.9532 | 17.5012 | 588.8803 | 23.0747 | -13.4489 | 589.4199 | -21.2911 | -15.7665 | 589.1768 |
| | 1 | 4.8177 | 17.0521 | 580.1771 | 26.4437 | -11.2979 | 585.9768 | -19.8005 | -11.4379 | 583.1299 |
| | 2 | 4.5388 | 17.9177 | 580.9418 | 26.9401 | -9.8933 | 586.2901 | -19.277 | -11.1959 | 584.7372 |
| 5 | 3 | 5.5142 | 17.6618 | 583.0452 | 27.3285 | -10.7044 | 587.4915 | -18.9385 | -11.1545 | 585.4228 |
| | 4 | 5.6732 | 16.0835 | 582.1924 | 27.5646 | -12.3044 | 586.6581 | -18.5598 | -12.6465 | 584.6339 |
| | 5 | 4.4431 | 15.7198 | 580.5497 | 25.7065 | -12.9752 | 586.1041 | -20.4566 | -12.4813 | 584.2786 |

Supplementary table 2. Naïve data – coordinates of virtual mounting



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| | 1 | 8.2617 | 9.7893 | 584.3655 | 27.0161 | -16.6029 | 592.037 | -21.8455 | -14.1485 | 590.6295 |
|----|---|--------|---------|----------|---------|----------|----------|----------|----------|----------|
| | 2 | 8.7739 | 9.6446 | 585.5703 | 25.8143 | -17.5644 | 590.9478 | -23.0683 | -14.7992 | 588.8892 |
| 6 | 3 | 6.5307 | 9.3445 | 586.064 | 27.6118 | -18.5394 | 591.3278 | -21.3222 | -15.8166 | 589.3813 |
| | 4 | 6.0744 | 9.0865 | 584.8301 | 27.4547 | -15.433 | 592.8502 | -21.4127 | -14.3772 | 590.51 |
| | 5 | 8.2593 | 9.756 | 584.6374 | 25.5161 | -13.7828 | 589.9416 | -23.3842 | -12.0393 | 589.3584 |
| | 1 | 5.6351 | 20.4533 | 587.0933 | 28.8083 | -7.8677 | 588.302 | -23.954 | -8.6506 | 584.5223 |
| | 2 | 5.1162 | 20.8818 | 588.4581 | 27.5616 | -8.1016 | 589.4565 | -25.2224 | -7.4018 | 585.2328 |
| 7 | 3 | 2.1641 | 19.6144 | 588.3663 | 24.8923 | -9.1297 | 588.441 | -27.9213 | -8.8209 | 585.3202 |
| | 4 | 6.9437 | 17.6849 | 587.6008 | 29.2756 | -11.4187 | 587.4192 | -23.535 | -10.4727 | 584.4354 |
| | 5 | 4.7162 | 18.0445 | 588.696 | 27.3584 | -10.6455 | 588.0436 | -25.3214 | -10.5473 | 584.9702 |
| | 1 | 5.4838 | 17.838 | 585.3101 | 25.9295 | -10.4018 | 580.586 | -20.4379 | -15.3101 | 578.7899 |
| | 2 | 7.1435 | 18.3267 | 588.3475 | 27.549 | -9.9019 | 582.5602 | -18.8894 | -14.5907 | 580.4328 |
| 8 | 3 | 5.2771 | 18.4014 | 586.2206 | 25.3766 | -9.8886 | 579.9045 | -20.9853 | -14.462 | 579.4915 |
| | 4 | 5.6969 | 17.8162 | 587.7831 | 25.8552 | -10.6689 | 583.0134 | -20.5116 | -14.9498 | 581.2211 |
| | 5 | 5.5638 | 19.2257 | 586.185 | 26.0255 | -9.1435 | 581.1868 | -20.5306 | -13.8077 | 579.2355 |
| | 1 | 5.5201 | 14.2758 | 583.8799 | 25.0178 | -7.9091 | 586.8351 | -26.6656 | -7.4655 | 583.1929 |
| | 2 | 6.3878 | 12.1554 | 584.3997 | 26.1587 | -9.6364 | 587.5553 | -25.5088 | -10.0282 | 583.6755 |
| 9 | 3 | 4.166 | 13.405 | 582.4732 | 23.7594 | -8.5868 | 585.2891 | -27.9589 | -8.3453 | 582.1067 |
| | 4 | 0.3483 | 14.391 | 583.7759 | 20.3981 | -7.0827 | 586.6002 | -31.2561 | -8.1089 | 583.4102 |
| | 5 | 5.1957 | 11.6659 | 583.5278 | 24.2805 | -10.7574 | 586.4762 | -27.462 | -9.3853 | 584.1177 |
| | 1 | 6.7053 | 6.529 | 589.8192 | 24.3956 | -8.577 | 588.7211 | -14.5574 | -12.2465 | 587.0787 |
| | 2 | 6.2793 | 5.4238 | 589.8259 | 23.7072 | -10.0345 | 588.9439 | -15.2911 | -13.1152 | 587.4274 |
| 10 | 3 | 5.5395 | 6.0043 | 590.8394 | 23.0741 | -9.368 | 590.4919 | -15.8522 | -12.5669 | 587.7353 |
| | 4 | 4.8563 | 4.6628 | 591.8199 | 22.2849 | -10.7792 | 590.525 | -16.7393 | -13.7235 | 589.6926 |
| | 5 | 4.8433 | 6.0239 | 590.7003 | 22.2695 | -9.4569 | 589.4424 | -16.9029 | -12.5628 | 588.578 |
| | 1 | 5.0537 | 17.8049 | 586.5838 | 28.3744 | -6.227 | 581.1126 | -24.357 | -11.5233 | 579.8447 |
| | 2 | 4.9856 | 16.5939 | 586.1882 | 28.6734 | -7.356 | 581.7326 | -23.9541 | -13.1443 | 579.3139 |
| 11 | 3 | 5.4757 | 16.9501 | 586.3549 | 29.7583 | -6.5326 | 581.806 | -22.7193 | -13.3019 | 579.0687 |
| | 4 | 4.7955 | 18.1348 | 586.6705 | 27.9399 | -6.0232 | 581.4864 | -24.5997 | -11.0797 | 579.7228 |
| | 5 | 3.1927 | 16.8696 | 585.5352 | 26.7362 | -7.3518 | 581.2821 | -25.9719 | -12.7168 | 579.6417 |



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| | 1 | 3.4269 | 8.3278 | 586.4499 | 21.8655 | -9.645 | 585.5177 | -24.4258 | -8.0424 | 583.459 |
|----|---|--------|---------|----------|---------|----------|----------|----------|----------|----------|
| | 2 | 5.2854 | 7.8284 | 587.493 | 24.1791 | -9.6967 | 587.006 | -22.1681 | -9.1564 | 583.6285 |
| 12 | 3 | 3.4267 | 6.5449 | 585.7848 | 21.9693 | -11.2435 | 585.5772 | -24.2303 | -10.1533 | 582.5431 |
| | 4 | 4.0912 | 7.7604 | 587.0719 | 22.6017 | -10.1651 | 586.8167 | -23.6474 | -8.5175 | 583.2355 |
| | 5 | 4.1755 | 6.9665 | 586.5758 | 22.7902 | -10.8355 | 585.8425 | -23.606 | -9.6412 | 583.4244 |
| | 1 | 7.266 | 9.7706 | 588.5129 | 23.6415 | -20.8947 | 593.16 | -18.2738 | -24.7478 | 596.3731 |
| | 2 | 4.4121 | 8.8236 | 587.6308 | 20.3712 | -21.9707 | 591.8859 | -21.4146 | -25.2204 | 596.038 |
| 13 | 3 | 6.3631 | 9.0907 | 587.9067 | 22.3924 | -21.5951 | 593.0141 | -19.4465 | -24.9292 | 596.4626 |
| | 4 | 6.4505 | 8.7811 | 589.5793 | 21.8839 | -22.2478 | 594.2503 | -20.0094 | -24.8993 | 597.6304 |
| | 5 | 7.6846 | 8.5969 | 587.1259 | 23.4951 | -22.1621 | 592.6693 | -18.4391 | -25.1145 | 595.9459 |
| | 1 | 5.0629 | 19.2358 | 588.6362 | 28.9638 | -5.2488 | 590.5138 | -19.7586 | -2.6263 | 583.9501 |
| | 2 | 5.4327 | 19.8942 | 588.1583 | 28.8018 | -4.9741 | 590.4121 | -19.8323 | -1.6586 | 583.7642 |
| 14 | 3 | 5.4653 | 19.1023 | 589.1308 | 28.6669 | -6.0628 | 590.7658 | -19.9073 | -1.9798 | 583.8586 |
| | 4 | 4.5617 | 18.0988 | 589.3571 | 27.3765 | -7.527 | 591.038 | -21.2461 | -2.791 | 584.7512 |
| | 5 | 3.76 | 19.7252 | 588.9634 | 27.8105 | -4.7273 | 590.8895 | -21.0443 | -2.4156 | 585.092 |
| | 1 | 3.2747 | 14.5624 | 592.658 | 21.4512 | -9.7365 | 591.5232 | -20.6455 | -12.9297 | 590.3452 |
| | 2 | 1.6177 | 14.4879 | 592.0629 | 19.4318 | -10.0392 | 590.8146 | -22.7431 | -12.6811 | 589.6466 |
| 15 | 3 | 2.9421 | 14.7669 | 593.5195 | 20.2822 | -10.0692 | 592.8698 | -21.7221 | -11.7203 | 588.27 |
| | 4 | 3.3764 | 16.7045 | 592.4259 | 21.3904 | -7.6156 | 591.1533 | -20.7323 | -10.5841 | 589.5833 |
| | 5 | 3.8962 | 15.9944 | 592.1402 | 21.7832 | -8.4601 | 591.4619 | -20.363 | -11.1592 | 589.2821 |



| Subject No. | D.' | # | 11 | # | 16 | #26 | | |
|-------------|---------|---------|---------|---------|---------|---------|---------|--|
| Subject No. | Pair | C(mm) | V(mm) | C(mm) | V(mm) | C(mm) | V(mm) | |
| | 1&2 | 1.9444 | 2.1833 | 2.0393 | 2.536 | 2.9546 | 2.5506 | |
| | 1&3 | 2.5094 | 1.2478 | 2.4861 | 1.5738 | 2.1205 | 1.099 | |
| | 1&4 | 4.868 | 2.2248 | 5.5554 | 2.5039 | 5.0383 | 2.1277 | |
| | 1&5 | 2.9798 | 1.2498 | 3.5497 | 1.0076 | 2.1363 | 1.0619 | |
| | 2&3 | 3.0532 | 2.9684 | 3.9152 | 3.2641 | 2.5594 | 2.8716 | |
| 1 | 2&4 | 6.3545 | 1.0424 | 7.0756 | 0.8299 | 7.2362 | 1.5513 | |
| | 2&5 | 3.9743 | 0.9566 | 4.0013 | 1.6775 | 3.895 | 1.566 | |
| | 3&4 | 6.7567 | 2.7438 | 6.502 | 3.0981 | 6.4267 | 2.4008 | |
| | 3&5 | 5.4627 | 2.1711 | 5.3665 | 2.2641 | 3.9566 | 1.607 | |
| | 4&5 | 3.3172 | 1.3906 | 4.0273 | 1.8827 | 3.719 | 1.7377 | |
| | Average | 4.12202 | 1.81786 | 4.45184 | 2.06377 | 4.00426 | 1.85736 | |
| | 1&2 | 4.392 | 3.0404 | 4.8397 | 3.1105 | 5.0427 | 3.0017 | |
| | 1&3 | 2.4306 | 2.3395 | 2.0737 | 1.3784 | 3.0594 | 1.3036 | |
| | 1&4 | 2.4818 | 1.4728 | 2.4894 | 1.6694 | 3.1154 | 1.5517 | |
| | 1&5 | 2.9001 | 2.2516 | 2.8885 | 2.7716 | 2.8648 | 2.0081 | |
| 2 | 2&3 | 6.4551 | 2.6681 | 6.1491 | 2.6957 | 6.4994 | 2.9146 | |
| Z | 2&4 | 6.1566 | 1.9479 | 6.2635 | 1.91 | 6.9839 | 2.2868 | |
| | 2&5 | 6.734 | 2.0334 | 7.0173 | 2.2375 | 7.0883 | 2.2514 | |
| | 3&4 | 0.8143 | 2.237 | 1.0761 | 1.3555 | 2.1959 | 1.052 | |
| | 3&5 | 0.7071 | 1.5822 | 0.9081 | 2.8321 | 1.4444 | 2.7606 | |
| | 4&5 | 0.5952 | 1.2382 | 1.4979 | 1.4906 | 1.134 | 2.0786 | |
| | Average | 3.36668 | 2.08111 | 3.52033 | 2.14513 | 3.94282 | 2.12091 | |
| | 1&2 | 5.7496 | 2.6995 | 5.9923 | 2.7661 | 4.0898 | 2.571 | |
| | 1&3 | 6.432 | 1.0445 | 7.3714 | 1.1062 | 5.689 | 1.2347 | |
| 3 | 1&4 | 3.0007 | 1.9787 | 3.5431 | 2.3689 | 1.4447 | 2.609 | |
| | 1&5 | 7.4918 | 0.8171 | 8.8869 | 0.6855 | 6.3326 | 0.5142 | |
| | 2&3 | 3.6417 | 1.8492 | 3.1734 | 1.9651 | 3.4214 | 1.6395 | |

Supplementary table 3. Distance between target points with each mounting technique



| | 2&4 | 4.9702 | 3.1492 | 3.8574 | 2.6507 | 3.8281 | 3.4926 |
|---|---------|---------|---------|---------|---------|---------|---------|
| | 2&5 | 5.8199 | 2.6522 | 4.8378 | 2.2913 | 5.7056 | 2.4856 |
| | 3&4 | 6.1261 | 2.1992 | 5.7702 | 1.6491 | 5.4841 | 2.1326 |
| | 3&5 | 5.7963 | 1.1729 | 5.5344 | 1.0309 | 5.3537 | 1.009 |
| | 4&5 | 4.9228 | 2.7635 | 5.4755 | 2.5846 | 5.0781 | 2.208 |
| | Average | 5.39511 | 2.0326 | 5.44424 | 1.90984 | 4.64271 | 1.98962 |
| | 1&2 | 4.3952 | 1.6054 | 4.0298 | 2.2073 | 5.7798 | 2.8033 |
| | 1&3 | 5.9959 | 2.5815 | 5.1828 | 3.9529 | 7.2094 | 3.7478 |
| | 1&4 | 1.9502 | 0.9693 | 1.6322 | 2.0791 | 2.268 | 1.3441 |
| | 1&5 | 8.0454 | 4.2053 | 7.8755 | 4.436 | 8.0983 | 4.8106 |
| | 2&3 | 1.7875 | 2.1365 | 1.5031 | 1.9371 | 1.777 | 2.0313 |
| 4 | 2&4 | 2.9479 | 2.1786 | 2.7285 | 2.7805 | 3.8999 | 3.3809 |
| | 2&5 | 5.958 | 2.7751 | 7.1374 | 2.2862 | 6.7072 | 2.3516 |
| | 3&4 | 4.2843 | 2.4293 | 3.6852 | 3.6153 | 5.1177 | 3.9282 |
| | 3&5 | 4.9697 | 2.6086 | 6.3295 | 1.9233 | 6.3372 | 1.5886 |
| | 4&5 | 6.1884 | 4.5131 | 6.6143 | 4.8886 | 6.25 | 5.2364 |
| | Average | 4.65225 | 2.60027 | 4.67183 | 3.01063 | 5.34445 | 3.12228 |
| | 1&2 | 5.4344 | 1.1882 | 5.6751 | 1.5224 | 6.2285 | 1.7076 |
| | 1&3 | 5.8857 | 3.0137 | 6.7542 | 1.8519 | 5.2279 | 2.4659 |
| | 1&4 | 3.0022 | 2.394 | 3.0206 | 1.6533 | 3.6299 | 2.2939 |
| | 1&5 | 5.2668 | 1.4333 | 5.689 | 1.8366 | 5.0847 | 1.6848 |
| | 2&3 | 8.1892 | 2.3326 | 8.7421 | 1.5007 | 7.4215 | 0.7658 |
| 5 | 2&4 | 3.7059 | 2.493 | 4.1433 | 2.5176 | 4.147 | 1.6215 |
| | 2&5 | 7.0588 | 2.2347 | 7.2205 | 3.3249 | 6.856 | 1.8038 |
| | 3&4 | 5.4513 | 1.801 | 5.8549 | 1.8194 | 4.5758 | 1.7297 |
| | 3&5 | 1.4146 | 3.3386 | 1.7474 | 3.1164 | 0.7847 | 2.3182 |
| | 4&5 | 4.7494 | 2.0842 | 4.7878 | 2.0516 | 4.3784 | 1.9368 |
| | Average | 5.01583 | 2.23133 | 5.36349 | 2.11948 | 4.83344 | 1.8328 |
| | 1&2 | 1.9974 | 2.0609 | 1.8484 | 1.8856 | 1.3172 | 2.2242 |
| 6 | 1&3 | 2.6301 | 2.542 | 2.1332 | 2.1466 | 2.4656 | 2.1481 |
| | 1&4 | 0.7261 | 0.6877 | 1.4434 | 1.4907 | 2.3439 | 0.5039 |



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| | 1&5 | 3.4487 | 3.5785 | 3.8145 | 3.8202 | 0.274 | 2.9038 |
|---|---------|---------|---------|---------|---------|---------|---------|
| | 2&3 | 1.8377 | 1.8596 | 1.9 | 2.08 | 2.3164 | 2.08 |
| | 2&4 | 1.7761 | 1.8138 | 3.2379 | 3.2944 | 2.8543 | 2.355 |
| | 2&5 | 3.712 | 3.7092 | 3.9975 | 3.9245 | 1.0712 | 2.8172 |
| | 3&4 | 2.5705 | 2.5848 | 3.4125 | 3.4629 | 1.3406 | 1.8314 |
| | 3&5 | 5.286 | 5.3143 | 5.345 | 5.3795 | 2.2788 | 4.3036 |
| | 4&5 | 3.059 | 3.0956 | 3.8808 | 3.8654 | 2.2933 | 3.2678 |
| | Average | 2.70436 | 1.85553 | 3.10132 | 3.13498 | 2.42264 | 2.4435 |
| | 1&2 | 6.3787 | 1.5217 | 5.3016 | 1.7152 | 6.2255 | 1.9166 |
| | 1&3 | 5.2077 | 3.791 | 6.1321 | 4.1167 | 6.6574 | 4.0503 |
| | 1&4 | 6.6633 | 3.1038 | 5.3479 | 3.6888 | 7.7114 | 1.8716 |
| | 1&5 | 4.6412 | 3.0357 | 6.2337 | 3.1441 | 6.8981 | 2.3807 |
| | 2&3 | 3.2403 | 3.2139 | 3.6202 | 3.0353 | 6.5494 | 3.0505 |
| 7 | 2&4 | 4.2148 | 3.7808 | 4.9207 | 4.2534 | 5.8028 | 3.5935 |
| | 2&5 | 3.185 | 2.8752 | 5.1252 | 2.917 | 5.2696 | 3.158 |
| | 3&4 | 1.8662 | 5.2108 | 2.2548 | 5.0494 | 2.2483 | 4.7697 |
| | 3&5 | 0.9672 | 3.0143 | 3.1483 | 2.9218 | 3.2872 | 3.1404 |
| | 4&5 | 2.8234 | 2.5081 | 2.0688 | 2.1594 | 1.9794 | 1.8662 |
| | Average | 3.91878 | 3.20553 | 4.41533 | 3.30011 | 5.26291 | 2.97975 |
| | 1&2 | 1.8016 | 3.4956 | 2.269 | 2.602 | 2.0661 | 2.3695 |
| | 1&3 | 5.3536 | 1.0905 | 7.6924 | 1.0166 | 4.1794 | 1.2292 |
| | 1&4 | 2.3262 | 2.4823 | 1.6974 | 2.4431 | 2.023 | 2.4589 |
| | 1&5 | 6.6072 | 1.6423 | 6.1653 | 1.3977 | 4.8708 | 1.5698 |
| | 2&3 | 4.0885 | 2.8307 | 6.124 | 3.4311 | 3.6867 | 2.3012 |
| 8 | 2&4 | 1.5968 | 1.6346 | 2.8247 | 1.9138 | 1.3096 | 1.839 |
| | 2&5 | 4.8928 | 2.8249 | 5.2662 | 2.1869 | 3.3345 | 2.1772 |
| | 3&4 | 5.2161 | 1.7206 | 7.7852 | 3.2408 | 4.8296 | 1.8585 |
| | 3&5 | 4.454 | 0.8734 | 4.1934 | 1.6188 | 4.0003 | 0.8369 |
| | 4&5 | 4.8087 | 2.135 | 5.3682 | 2.3859 | 3.8513 | 2.2907 |
| | Average | 4.11455 | 2.07299 | 4.93858 | 2.22367 | 3.41513 | 1.89309 |
| | 1&2 | 1.8739 | 2.3493 | 2.4215 | 2.1917 | 1.7811 | 2.8528 |



| | 1&3 | 3.4276 | 2.1379 | 6.3252 | 2.1054 | 1.9381 | 1.9043 |
|----|---------|---------|---------|---------|---------|---------|---------|
| | 1&4 | 4.0843 | 5.1742 | 4.485 | 4.6989 | 4.6114 | 4.6405 |
| | 1&5 | 5.5124 | 2.6535 | 7.0188 | 2.964 | 6.3281 | 2.2748 |
| | 2&3 | 2.1466 | 3.1952 | 5.2593 | 3.4632 | 1.7834 | 3.3611 |
| 0 | 2&4 | 4.1661 | 6.4702 | 4.8851 | 6.3732 | 5.6993 | 6.0652 |
| 9 | 2&5 | 4.6493 | 1.556 | 6.547 | 2.439 | 6.5002 | 2.1033 |
| | 3&4 | 3.1041 | 4.1526 | 3.4596 | 3.9089 | 4.0848 | 3.5534 |
| | 3&5 | 3.4509 | 2.2797 | 2.7065 | 2.5283 | 4.807 | 2.3179 |
| | 4&5 | 3.2421 | 5.5665 | 3.1112 | 5.3471 | 3.5949 | 4.0651 |
| | Average | 3.56573 | 3.55351 | 4.62192 | 3.60197 | 4.11283 | 3.31384 |
| | 1&2 | 8.1886 | 1.1845 | 9.4449 | 1.6272 | 8.1122 | 1.1894 |
| | 1&3 | 6.2337 | 1.6356 | 6.5828 | 2.3469 | 6.6567 | 1.4867 |
| 10 | 1&4 | 7.5747 | 3.3022 | 9.0002 | 3.5439 | 8.327 | 3.7114 |
| | 1&5 | 8.3503 | 2.121 | 9.2979 | 2.4114 | 8.5057 | 2.8017 |
| | 2&3 | 2.7411 | 1.3826 | 3.5668 | 1.8003 | 1.9804 | 0.8428 |
| | 2&4 | 5.1481 | 2.5652 | 5.1129 | 2.2533 | 5.3039 | 2.7565 |
| 10 | 2&5 | 2.9529 | 1.7852 | 3.593 | 1.6276 | 4.1592 | 2.0559 |
| | 3&4 | 3.9531 | 1.7966 | 4.4211 | 1.6172 | 3.9319 | 2.4404 |
| | 3&5 | 4.272 | 0.7102 | 4.7348 | 1.3254 | 4.2033 | 1.3469 |
| | 4&5 | 4.3026 | 1.7625 | 3.0897 | 1.709 | 5.1132 | 1.6175 |
| | Average | 5.37171 | 1.82456 | 5.88441 | 2.02622 | 5.62935 | 2.02492 |
| | 1&2 | 3.7865 | 1.2759 | 4.274 | 1.3224 | 4.1535 | 1.7527 |
| | 1&3 | 2.1832 | 0.9804 | 2.5927 | 1.5778 | 2.0697 | 2.5393 |
| | 1&4 | 3.4417 | 0.4278 | 4.1493 | 0.6083 | 5.2638 | 0.5201 |
| | 1&5 | 5.7024 | 2.3319 | 6.7009 | 1.9944 | 5.0949 | 2.0183 |
| 11 | 2&3 | 3.1938 | 0.6284 | 3.1096 | 1.364 | 2.8785 | 1.2688 |
| 11 | 2&4 | 6.9101 | 1.6258 | 7.9843 | 1.5411 | 8.9628 | 2.2015 |
| | 2&5 | 5.7666 | 1.928 | 5.6749 | 1.9889 | 4.8467 | 2.0885 |
| | 3&4 | 4.1362 | 1.4021 | 5.5797 | 1.9153 | 6.3002 | 2.9836 |
| | 3&5 | 3.7378 | 2.4271 | 4.2673 | 3.1747 | 3.4656 | 3.3541 |
| | 4&5 | 5.8471 | 2.3364 | 8.1415 | 1.8044 | 6.8763 | 2.1377 |



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| | Average | 4.47054 | 1.53638 | 5.24742 | 1.72913 | 4.9912 | 2.08646 |
|----|---------|---------|---------|---------|---------|---------|---------|
| | 1&2 | 11.2338 | 2.189 | 11.0033 | 2.7514 | 10.2422 | 2.5233 |
| | 1&3 | 1.8245 | 1.903 | 1.1433 | 1.603 | 1.349 | 2.3094 |
| | 1&4 | 5.7352 | 1.0725 | 4.9773 | 1.5811 | 5.6485 | 0.939 |
| | 1&5 | 5.9288 | 1.5587 | 5.6498 | 1.5421 | 4.9562 | 1.7971 |
| | 2&3 | 10.8275 | 2.832 | 11.7414 | 3.0524 | 10.0976 | 2.5347 |
| 12 | 2&4 | 5.6997 | 1.2681 | 6.238 | 1.6563 | 4.8155 | 1.6586 |
| | 2&5 | 10.0541 | 1.6781 | 10.1716 | 2.14 | 10.7067 | 1.5311 |
| | 3&4 | 5.4181 | 1.891 | 5.776 | 1.7604 | 5.5523 | 1.8696 |
| | 3&5 | 5.6036 | 1.1679 | 5.2217 | 0.9543 | 4.7992 | 1.1953 |
| | 4&5 | 6.9381 | 0.94 | 6.2954 | 1.1975 | 7.6349 | 1.1402 |
| | Average | 6.92634 | 1.65003 | 6.82178 | 1.82385 | 6.58021 | 1.74983 |
| | 1&2 | 17.166 | 3.1336 | 18.0952 | 3.671 | 17.4401 | 3.1938 |
| | 1&3 | 10.0499 | 1.2825 | 11.4094 | 1.4395 | 10.4522 | 1.1901 |
| | 1&4 | 9.1695 | 1.6677 | 10.9571 | 2.4715 | 12.2658 | 2.1485 |
| | 1&5 | 10.2163 | 1.8645 | 12.5206 | 1.367 | 11.5094 | 0.5867 |
| | 2&3 | 8.5878 | 1.9885 | 9.2342 | 2.3451 | 8.9348 | 2.0344 |
| 13 | 2&4 | 9.1261 | 2.8202 | 9.7145 | 2.8206 | 8.8709 | 2.1479 |
| | 2&5 | 7.5628 | 3.3189 | 7.4956 | 3.2263 | 7.9737 | 2.9789 |
| | 3&4 | 3.4131 | 1.7033 | 3.0453 | 1.4875 | 3.7845 | 1.2966 |
| | 3&5 | 2.9491 | 1.6123 | 2.7594 | 1.287 | 3.1786 | 1.1473 |
| | 4&5 | 1.6298 | 2.7524 | 2.3282 | 2.2589 | 1.6374 | 2.3129 |
| | Average | 7.98704 | 2.21439 | 8.75595 | 2.23744 | 8.60474 | 1.90371 |
| | 1&2 | 3.8457 | 0.8937 | 5.2745 | 0.3347 | 6.1411 | 0.9881 |
| | 1&3 | 6.3038 | 0.6514 | 6.9 | 0.9024 | 6.5031 | 0.6696 |
| | 1&4 | 5.0882 | 1.4366 | 6.2349 | 2.8256 | 5.2886 | 1.6975 |
| 1/ | 1&5 | 7.5222 | 1.4298 | 7.2658 | 1.3203 | 6.5422 | 1.7324 |
| 14 | 2&3 | 8.1944 | 1.2546 | 10.2994 | 1.1526 | 11.2603 | 0.343 |
| | 2&4 | 6.6332 | 2.328 | 10.0917 | 2.99 | 10.2965 | 2.0628 |
| | 2&5 | 8.3211 | 1.864 | 10.3192 | 1.1275 | 10.4291 | 1.9506 |
| | 3&4 | 4.6181 | 1.3692 | 5.3949 | 1.9705 | 4.019 | 1.802 |



| | 3&5 | 7.0936 | 1.8232 | 7.4448 | 1.5913 | 6.4637 | 1.7332 |
|----|---------|---------|---------|---------|---------|---------|---------|
| | 4&5 | 2.9151 | 1.8555 | 2.3295 | 2.8371 | 2.7242 | 0.5458 |
| | Average | 6.05354 | 1.4906 | 7.15547 | 1.7052 | 6.96678 | 1.3525 |
| | 1&2 | 2.5503 | 1.7621 | 2.0583 | 2.1614 | 2.918 | 2.2248 |
| | 1&3 | 2.963 | 0.9458 | 2.0048 | 1.814 | 4.9734 | 2.6321 |
| | 1&4 | 1.4927 | 2.157 | 3.0011 | 2.1538 | 3.8867 | 2.4678 |
| | 1&5 | 3.9617 | 1.6447 | 3.029 | 1.3203 | 5.3642 | 2.0844 |
| 15 | 2&3 | 4.1 | 1.9883 | 3.4826 | 2.2244 | 3.842 | 1.9649 |
| 15 | 2&4 | 3.6743 | 2.8527 | 4.7012 | 3.1344 | 3.5242 | 2.9059 |
| | 2&5 | 3.9714 | 2.7326 | 2.8074 | 2.9055 | 3.3568 | 2.8485 |
| | 3&4 | 2.9564 | 2.2669 | 2.7173 | 3.1928 | 3.262 | 1.9987 |
| | 3&5 | 1.8426 | 2.0783 | 2.4736 | 2.6123 | 1.7214 | 1.785 |
| | 4&5 | 4.4212 | 0.9253 | 4.5839 | 0.9812 | 4.1496 | 0.7468 |
| | Average | 3.19336 | 1.93537 | 3.08592 | 2.25001 | 3.69983 | 2.16589 |

The number written in the pair column means the order of trial.



| Subject | Cx(mm) | Vx(mm) | Cy(mm) | Vy(mm) | Cz(mm) | Vz(mm) |
|---------|----------|---------|----------|---------|----------|---------|
| 1 | 2.210066 | 0.93116 | 1.39294 | 0.87948 | 0.980414 | 0.50069 |
| 2 | 1.544389 | 1.0409 | 2.318215 | 0.63298 | 0.742219 | 0.90445 |
| 3 | 1.457772 | 0.76899 | 2.79142 | 0.93172 | 2.328236 | 0.94846 |
| 4 | 2.166371 | 1.36709 | 2.590722 | 0.74577 | 1.105329 | 1.21349 |
| 5 | 1.625976 | 0.56428 | 2.340377 | 0.96149 | 2.48396 | 1.20013 |
| 6 | 1.00021 | 1.19577 | 1.699389 | 0.30099 | 0.699291 | 0.70296 |
| 7 | 0.723325 | 1.75226 | 1.956665 | 1.42386 | 2.208107 | 0.67095 |
| 8 | 0.656215 | 0.74823 | 2.533205 | 0.57295 | 1.694005 | 1.25402 |
| 9 | 1.250357 | 2.36013 | 1.186667 | 1.23088 | 1.981585 | 0.71117 |
| 10 | 2.321245 | 0.83703 | 1.749811 | 0.71286 | 2.820813 | 0.83132 |
| 11 | 2.454289 | 0.87884 | 2.105245 | 0.66215 | 0.735753 | 0.45073 |
| 12 | 2.337536 | 0.76085 | 4.12688 | 0.71706 | 2.31699 | 0.648 |
| 13 | 2.132615 | 1.25992 | 1.286471 | 0.45902 | 5.904661 | 0.94236 |
| 14 | 1.218226 | 0.71317 | 2.591073 | 0.70367 | 3.417433 | 0.46718 |
| 15 | 0.827929 | 0.85617 | 1.68337 | 0.99279 | 1.424566 | 0.58557 |

Supplementary table 4. Standard deviation of each coordinates for #11

C, conventional mounting technique; V, virtual mounting technique



| Subject | Cx(mm) | Vx(mm) | Cy(mm) | Vy(mm) | Cz(mm) | Vz(mm) |
|---------|----------|---------|----------|---------|----------|----------|
| 1 | 2.241631 | 0.76116 | 1.610891 | 1.05948 | 1.131465 | 0.85386 |
| 2 | 1.55481 | 1.08543 | 2.361391 | 0.60652 | 0.803304 | 0.977837 |
| 3 | 1.492335 | 0.70429 | 3.267595 | 0.86503 | 1.815925 | 0.912991 |
| 4 | 2.577589 | 1.84975 | 2.55643 | 0.74946 | 0.334703 | 1.053832 |
| 5 | 1.868275 | 0.74266 | 2.279219 | 1.2306 | 2.753088 | 0.608793 |
| 6 | 0.921409 | 0.95988 | 1.855612 | 1.85457 | 1.097809 | 1.100375 |
| 7 | 0.98525 | 1.70711 | 1.921892 | 1.55948 | 2.477339 | 0.74055 |
| 8 | 1.591128 | 0.82255 | 3.208689 | 0.58406 | 1.201988 | 1.311593 |
| 9 | 1.146425 | 2.16659 | 1.390512 | 1.44214 | 2.946649 | 0.820021 |
| 10 | 2.400035 | 0.92078 | 1.610838 | 0.82019 | 3.43643 | 0.847908 |
| 11 | 3.033066 | 1.10076 | 2.384834 | 0.62549 | 0.728815 | 0.29334 |
| 12 | 2.165355 | 0.92656 | 4.457238 | 0.70475 | 1.850047 | 0.707047 |
| 13 | 2.726862 | 1.33358 | 1.256883 | 0.55204 | 6.372811 | 0.857255 |
| 14 | 1.265226 | 0.69222 | 2.848114 | 1.13423 | 4.342858 | 0.259422 |
| 15 | 1.172638 | 0.98189 | 1.552912 | 1.09591 | 1.168933 | 0.782221 |

| Supplementary table 5. Standard | d deviation of each | coordinates for #16 |
|---------------------------------|---------------------|---------------------|
|---------------------------------|---------------------|---------------------|

C, conventional mounting technique; V, virtual mounting technique



| Subject | Cx(mm) | Vx(mm) | Cy(mm) | Vy(mm) | Cz(mm) | Vz(mm) |
|---------|----------|----------|----------|----------|----------|----------|
| 1 | 2.246858 | 0.76204 | 1.112213 | 0.80138 | 1.111982 | 0.81793 |
| 2 | 1.586507 | 1.10062 | 2.214741 | 0.615124 | 1.638771 | 0.927275 |
| 3 | 1.436077 | 0.68353 | 2.399139 | 1.138145 | 1.979313 | 0.756899 |
| 4 | 2.631497 | 1.885858 | 3.023672 | 0.990363 | 0.42013 | 1.062247 |
| 5 | 1.864425 | 0.743411 | 2.322762 | 0.723196 | 2.094456 | 0.841759 |
| 6 | 0.960196 | 0.958137 | 1.358535 | 1.38461 | 0.77364 | 0.771576 |
| 7 | 0.979272 | 1.713551 | 2.268616 | 1.333397 | 3.099446 | 0.403327 |
| 8 | 1.626708 | 0.801901 | 1.828128 | 0.563599 | 0.720192 | 0.980849 |
| 9 | 1.0893 | 2.157323 | 1.159483 | 1.028031 | 2.722594 | 0.751201 |
| 10 | 2.358225 | 0.985002 | 1.98704 | 0.58308 | 2.917493 | 1.048008 |
| 11 | 3.165723 | 1.173083 | 2.024389 | 0.996069 | 0.441337 | 0.31918 |
| 12 | 2.218095 | 0.884681 | 3.616017 | 0.846067 | 2.785817 | 0.423364 |
| 13 | 2.784798 | 1.280208 | 1.325475 | 0.186325 | 6.145281 | 0.673661 |
| 14 | 1.196102 | 0.72431 | 2.31899 | 0.46762 | 4.590952 | 0.598703 |
| 15 | 1.197142 | 0.983875 | 1.878922 | 0.993333 | 1.535132 | 0.754218 |

Supplementary table 6. Standard deviation of each coordinates for #26

C, conventional mounting technique; V, virtual mounting technique



| Order of Repetition | Subject | Cx | Vx | Су | Vy | Cz | Vz |
|------------------------|---------|---------|--------|---------|---------|----------|----------|
| | 1 | 1.7104 | 2.8611 | 1.34 | 14.7741 | 585.2681 | 587.9949 |
| | 2 | 1.527 | 3.0286 | 10.7433 | 15.568 | 579.2816 | 576.266 |
| | 3 | 6.1582 | 6.4436 | 4.9126 | 13.0757 | 591.2545 | 588.3946 |
| | 4 | 5.8202 | 7.9869 | 15.3797 | 16.9227 | 591.6124 | 586.0261 |
| | 5 | 3.4836 | 4.8177 | 9.2698 | 17.0521 | 586.312 | 580.1771 |
| | 6 | 6.6678 | 8.2617 | 10.1602 | 9.7893 | 586.442 | 584.3655 |
| | 7 | 5.686 | 5.6351 | 12.3615 | 20.4533 | 587.6111 | 587.0933 |
| 1 | 8 | 4.4131 | 5.4838 | 12.9498 | 17.838 | 586.9499 | 585.3101 |
| | 9 | 6.1753 | 5.5201 | 10.0438 | 14.2758 | 591.059 | 583.8799 |
| | 10 | 7.9874 | 6.7053 | -5.9247 | 6.529 | 584.3834 | 589.8192 |
| | 11 | 4.0703 | 5.0537 | 6.657 | 17.8049 | 592.9933 | 586.5838 |
| | 12 | 5.7459 | 3.4269 | -3.3492 | 8.3278 | 590.647 | 586.4499 |
| | 13 | 10.4638 | 7.266 | 5.2973 | 9.7706 | 580.0813 | 588.5129 |
| | 14 | 4.0403 | 5.0629 | 12.1093 | 19.2358 | 594.1094 | 588.6362 |
| | 15 | 4.3357 | 3.2747 | 4.0699 | 14.5624 | 590.0557 | 592.658 |
| | 1 | 2.9852 | 1.165 | 2.2881 | 16.1205 | 584.1472 | 588.2723 |
| | 2 | 4.8214 | 0.1446 | 13.4005 | 16.5292 | 578.1086 | 576.2157 |
| | 3 | 4.6815 | 8.2233 | 9.3873 | 15.093 | 594.5491 | 588.1695 |
| | 4 | 6.47 | 7.2988 | 11.6125 | 17.3815 | 593.7813 | 587.402 |
| | 5 | 7.5079 | 4.5388 | 5.934 | 17.9177 | 587.7987 | 580.9418 |
| | 6 | 6.054 | 8.7739 | 9.1981 | 9.6446 | 584.8027 | 585.5703 |
| | 7 | 6.4459 | 5.1162 | 17.8886 | 20.8818 | 590.7034 | 588.4581 |
| 2 | 8 | 4.2609 | 7.1435 | 11.4545 | 18.3267 | 585.9567 | 588.3475 |
| | 9 | 6.6893 | 6.3878 | 11.7122 | 12.1554 | 590.3781 | 584.3997 |
| | 10 | 1.895 | 6.2793 | -5.7358 | 5.4238 | 589.8515 | 589.8259 |
| | 11 | 7.855 | 4.9856 | 6.7308 | 16.5939 | 593.0864 | 586.1882 |
| | 12 | 4.7565 | 5.2854 | 6.3646 | 7.8284 | 585.0916 | 587.493 |
| | 13 | 5.8148 | 4.4121 | 4.6681 | 8.8236 | 596.5938 | 587.6308 |
| | 14 | 7.1714 | 5.4327 | 11.3195 | 19.8942 | 596.1979 | 588.1583 |
| | 15 | 6.2255 | 1.6177 | 5.2567 | 14.4879 | 588.8212 | 592.0629 |
| | 1 | 2.8432 | 2.7115 | -0.7462 | 13.8259 | 584.4546 | 587.1978 |
| | 2 | 1.0247 | 1.8779 | 8.3787 | 16.1698 | 579.535 | 578.212 |
| | 3 | 8.1705 | 7.3819 | 10.3241 | 13.4973 | 594.0894 | 588.576 |
| | 4 | 5.9061 | 5.7679 | 9.9658 | 15.9663 | 594.188 | 586.9348 |
| С | 5 | 6.4996 | 5.5142 | 11.2731 | 17.6618 | 581.6717 | 583.0452 |
| 2 | 6 | 7.5587 | 6.5307 | 8.1592 | 9.3445 | 584.9859 | 586.064 |
| | 7 | 6.1201 | 2.1641 | 14.9791 | 19.6144 | 592.0922 | 588.3663 |
| | 8 | 4.1975 | 5.2771 | 7.6167 | 18.4014 | 587.3652 | 586.2206 |
| | 9 | 6.4316 | 4.166 | 12.0183 | 13.405 | 588.269 | 582.4732 |
| | 10 | 3.0475 | 5.5395 | -4.2998 | 6.0043 | 587.8209 | 590.8394 |

Supplementary table 7. Coordinate values of #11 according to the number of trials



| | 11 | 5.2415 | 5.4757 | 8.1975 | 16.9501 | 591.9824 | 586.3549 |
|---|----|---------|--------|---------|---------|----------|----------|
| | 12 | 5.0075 | 3.4267 | -3.7218 | 6.5449 | 589.0207 | 585.7848 |
| | 13 | 10.6122 | 6.3631 | 7.2212 | 9.0907 | 589.9442 | 587.9067 |
| | 14 | 6.225 | 5.4653 | 14.6841 | 19.1023 | 588.7863 | 589.1308 |
| | 15 | 4.2454 | 2.9421 | 5.9503 | 14.7669 | 592.3437 | 593.5195 |
| | 1 | -2.9666 | 0.7431 | 2.1246 | 15.2014 | 586.3671 | 588.5252 |
| | 2 | 1.7764 | 2.0794 | 8.3393 | 16.6715 | 579.8455 | 576.0414 |
| | 3 | 4.7233 | 7.0884 | 7.2603 | 12.623 | 590.0572 | 586.5795 |
| | 4 | 5.1423 | 7.9587 | 13.6079 | 15.9641 | 592.065 | 585.8848 |
| | 5 | 5.3056 | 5.6732 | 7.2111 | 16.0835 | 585.1056 | 582.1924 |
| | 6 | 6.788 | 6.0744 | 10.4731 | 9.0865 | 585.7979 | 584.8301 |
| | 7 | 7.2642 | 6.9437 | 14.904 | 17.6849 | 593.5647 | 587.6008 |
| 4 | 8 | 5.3446 | 5.6969 | 12.1158 | 17.8162 | 584.9882 | 587.7831 |
| | 9 | 6.5889 | 0.3483 | 9.1489 | 14.391 | 587.0955 | 583.7759 |
| | 10 | 5.1131 | 4.8563 | -1.7199 | 4.6628 | 589.99 | 591.8199 |
| | 11 | 1.1907 | 4.7955 | 8.5265 | 18.1348 | 592.7513 | 586.6705 |
| | 12 | 6.1279 | 4.0912 | 1.292 | 7.7604 | 587.2994 | 587.0719 |
| | 13 | 11.0165 | 6.4505 | 3.931 | 8.7811 | 589.1316 | 589.5793 |
| | 14 | 5.9093 | 4.5617 | 10.1864 | 18.0988 | 589.7852 | 589.3571 |
| | 15 | 4.411 | 3.3764 | 3.2017 | 16.7045 | 591.2676 | 592.4259 |
| | 1 | 0.0667 | 1.9868 | 3.4499 | 15.6604 | 586.5818 | 588.1052 |
| | 2 | 1.3616 | 1.8206 | 7.9297 | 17.2813 | 579.9649 | 577.0875 |
| | 3 | 5.2143 | 6.3297 | 12.1193 | 13.4825 | 589.438 | 589.0939 |
| | 4 | 1.1065 | 4.9532 | 9.0712 | 17.5012 | 593.2595 | 588.8803 |
| | 5 | 7.1131 | 4.4431 | 11.0214 | 15.7198 | 582.9213 | 580.5497 |
| | 6 | 4.8776 | 8.2593 | 12.7148 | 9.756 | 584.9714 | 584.6374 |
| | 7 | 5.406 | 4.7162 | 14.9696 | 18.0445 | 591.44 | 588.696 |
| 5 | 8 | 5.5936 | 5.5638 | 7.6851 | 19.2257 | 583.1362 | 586.185 |
| | 9 | 9.2333 | 5.1957 | 10.9474 | 11.6659 | 586.5624 | 583.5278 |
| | 10 | 4.1242 | 4.8433 | -5.508 | 6.0239 | 591.7745 | 590.7003 |
| | 11 | 5.806 | 3.1927 | 11.842 | 16.8696 | 591.3746 | 585.5352 |
| | 12 | 0.3302 | 4.1755 | -0.9513 | 6.9665 | 590.3802 | 586.5758 |
| | 13 | 9.9069 | 7.6846 | 4.373 | 8.5969 | 590.2405 | 587.1259 |
| | 14 | 6.8187 | 3.76 | 7.6155 | 19.7252 | 588.755 | 588.9634 |
| | 15 | 5.0148 | 3.8962 | 7.5449 | 15.9944 | 591.8329 | 592.1402 |

There is no unit because it is a coordinate value in space; C, conventional mounting technique; V, virtual mounting technique



| | VCandinata | 7 | = | | | 0 | 0 | |
|---|--------------|--------------|---|-----|-------------------------|----------|-----------|-----------------|
| | r Coordinate | Z coordinate | | | $\Lambda z / \Lambda v$ | θ | A | mean θc |
| 1 | 16.7378 | 650.785 | _ | | | (radian) | (degrees) | (degrees) |
| 2 | 5.2679 | 650.4512 | | 1&2 | 0.0291 | 0.0291 | 1.6670 | |
| 3 | -8.3294 | 650.6381 | | 1&3 | 0.0059 | 0.0059 | 0.3358 | |
| 4 | -21.3623 | 650.2887 | | 1&4 | 0.0130 | 0.0130 | 0.7463 | |
| 5 | -35.704 | 650.1708 | | 1&5 | 0.0117 | 0.0117 | 0.6710 | |
| | | | | 2&3 | -0.0138 | -0.0137 | -0.7875 | 0.025.00.4* |
| | | | | 2&4 | 0.0061 | 0.0061 | 0.3496 | 0.635894 |
| | | | | 2&5 | 0.0068 | 0.0068 | 0.3921 | |
| | | | | 3&4 | 0.0268 | 0.0268 | 1.5357 | |
| | | | | 3&5 | 0.0171 | 0.0171 | 0.9780 | |
| | | | | 4&5 | 0.0082 | 0.0082 | 0.4710 | |

Supplementary table 8. Angle between Y-axis and the Reference articulator

(Left) Set 5 points randomly on the horizontal reference plane of the Reference articulator and project in orthogonally on the YZ plane. There is no unit because it is a coordinate value in space. (**Right**) Calculate the average value after calculating the angle of the Y-axis and the line formed by two points in 10 pairs by the combination formula. Add the marked average value(*) to the mean θ value in Supplementary Table 9.



| | | | | Conventio | nal | | | | Virtual | | |
|-----|-------------------------|---------------------|---------------|----------------|--------------------|-----------------------|---------------------|-------------------|----------------|--------------------|-----------------------|
| No. | Order of Repetitions | $\Delta z/\Delta y$ | θ (radian) | θ (degrees) | SD θc (degrees) | mean θc (degrees)* | $\Delta z/\Delta y$ | θ (radian) | θ (degrees) | SD θv (degrees) | mean θv (degrees)* |
| | 1 | -0.1953 | -0.1929 | -11.053 | | | -0.0503 | -0.0502 | -2.8772 | | |
| | 2 | -0.2296 | -0.2257 | -12.931 | | | -0.0883 | -0.0881 | -5.0458 | | |
| 1 | 3 | -0.2569 | -0.2514 | -14.407 | 1.32442 | 13.7854 | -0.0744 | -0.0743 | -4.2554 | 1.3088 | 4.8780 |
| | 4 | -0.252 | -0.2469 | -14.145 | | | -0.1045 | -0.1041 | -5.9639 | | |
| | 5 | -0.2348 | -0.2306 | -13.211 | | | -0.0536 | -0.0536 | -3.0683 | | |
| | 1 | -0.2757 | -0.269 | -15.414 | | | -0.1514 | -0.1503 | -8.6105 | | |
| | 2 | -0.2786 | -0.2717 | -15.568 | | | -0.1365 | -0.1357 | -7.7747 | | |
| 2 | 3 | -0.2742 | -0.2676 | -15.334 | 0.72895 | 16.0654 | -0.1177 | -0.1172 | -6.7142 | 1.8777 | 7.6942 |
| | 4 | -0.2951 | -0.2869 | -16.44 | | | -0.1448 | -0.1438 | -8.2419 | | |
| | 5 | -0.2566 | -0.2512 | -14.392 | | | -0.0691 | -0.0689 | -3.9501 | | |
| | 1 | 0.06657 | 0.06647 | 3.8085 | | | 0.10829 | 0.10787 | 6.18071 | | |
| | 2 | 0.15165 | 0.1505 | 8.62324 | | | 0.12515 | 0.1245 | 7.13343 | | |
| 3 | 3 | 0.12397 | 0.12334 | 7.06682 | 1.95701 | -5.3877 | 0.13303 | 0.13225 | 7.57762 | 0.5140 | -6.324 |
| | 4 | 0.07748 | 0.07732 | 4.43016 | | | 0.11952 | 0.11895 | 6.81548 | | |
| | 5 | 0.10844 | 0.10802 | 6.1891 | | | 0.12438 | 0.12375 | 7.09031 | | |
| | 1 | -0.2151 | -0.2118 | -12.138 | | | -0.0663 | -0.0662 | -3.7925 | | |
| | 2 | -0.1161 | -0.1156 | -6.6209 | | | -0.0364 | -0.0364 | -2.0875 | | |
| 4 | 3 | -0.1084 | -0.108 | -6.1865 | 2.6041 | 9.300 | -0.0439 | -0.0439 | -2.5136 | 1.1239 | 2.7548 |
| | 4 | -0.1878 | -0.1856 | -10.637 | | | -0.021 | -0.021 | -1.2022 | | |
| | 5 | -0.1359 | -0.1351 | -7.7411 | | | -0.0174 | -0.0174 | -0.9988 | | |
| | 1 | -0.2438 | -0.2391 | -13.702 | | | -0.2046 | -0.2018 | -11.562 | | |
| | 2 | -0.2691 | -0.2629 | -15.064 | | | -0.1923 | -0.19 | -10.886 | | |
| 5 | 3 | -0.2346 | -0.2304 | -13.204 | 0.6847 | 14.6137 | -0.1567 | -0.1555 | -8.9084 | 1.2387 | 10.886 |
| | 4 | -0.2467 | -0.2419 | -13.859 | | | -0.1573 | -0.156 | -8.9399 | | |
| | 5 | -0.2504 | -0.2454 | -14.06 | | | -0.1936 | -0.1912 | -10.955 | | |
| | 1 | -0.2095 | -0.2065 | -11.834 | | | -0.2907 | -0.2829 | -16.208 | | |

Supplementary table 9. Angle of the occlusal plane



•

| | 2 | -0.23 | -0.2261 | -12.953 | | | -0.1976 | -0.1951 | -11.18 | | |
|----|---|---------|---------|---------|--------|---------|---------|---------|---------|--------|--------|
| 6 | 3 | -0.2375 | -0.2332 | -13.361 | 1 7152 | 12 4421 | -0.1888 | -0.1866 | -10.69 | 2 2459 | 1111 |
| 0 | 4 | -0.2722 | -0.2658 | -15.228 | 1./155 | 15.4421 | -0.3271 | -0.3161 | -18.112 | 5.2450 | 14.414 |
| | 5 | -0.1881 | -0.186 | -10.655 | | | -0.2253 | -0.2216 | -12.699 | | |
| | 1 | -0.1504 | -0.1493 | -8.554 | | | -0.0427 | -0.0427 | -2.4438 | | |
| | 2 | -0.0986 | -0.0983 | -5.6319 | | | -0.0344 | -0.0344 | -1.9729 | | |
| 7 | 3 | -0.1674 | -0.1658 | -9.5014 | 2.5286 | 9.1078 | -0.0026 | -0.0026 | -0.1489 | 1.5830 | 1.217 |
| | 4 | -0.1157 | -0.1152 | -6.6021 | | | 0.00624 | 0.00624 | 0.35751 | | |
| | 5 | -0.2138 | -0.2107 | -12.07 | | | 0.02274 | 0.02274 | 1.30266 | | |
| | 1 | 0.13822 | 0.13735 | 7.86952 | | | 0.16729 | 0.16575 | 9.4968 | | |
| | 2 | 0.05156 | 0.05152 | 2.95177 | | | 0.20502 | 0.20221 | 11.586 | | |
| 8 | 3 | 0.12099 | 0.12041 | 6.89877 | 2.1353 | -4.6854 | 0.22326 | 0.21966 | 12.5856 | 1.3868 | -9.997 |
| | 4 | 0.09572 | 0.09543 | 5.46782 | | | 0.16745 | 0.16591 | 9.50573 | | |
| | 5 | 0.05974 | 0.05966 | 3.41853 | | | 0.17618 | 0.17439 | 9.99206 | | |
| | 1 | -0.2275 | -0.2237 | -12.817 | | | -0.1332 | -0.1324 | -7.5876 | | |
| | 2 | -0.2508 | -0.2458 | -14.082 | | | -0.1448 | -0.1438 | -8.2395 | | |
| 9 | 3 | -0.1066 | -0.1062 | -6.0868 | 3.3633 | 11.2705 | -0.128 | -0.1274 | -7.2966 | 0.3614 | 8.2573 |
| | 4 | -0.2127 | -0.2096 | -12.009 | | | -0.1315 | -0.1308 | -7.4927 | | |
| | 5 | -0.1437 | -0.1427 | -8.1788 | | | -0.1315 | -0.1307 | -7.4907 | | |
| | 1 | 0.03641 | 0.03639 | 2.08527 | | | 0.07269 | 0.07257 | 4.15769 | | |
| | 2 | -0.0533 | -0.0533 | -3.0533 | | | 0.05706 | 0.05699 | 3.26557 | | |
| 10 | 3 | -0.2799 | -0.2729 | -15.637 | 8.5926 | 2.1551 | 0.02261 | 0.0226 | 1.29498 | 1.4360 | -2.996 |
| | 4 | 0.11425 | 0.11376 | 6.51769 | | | 0.08386 | 0.08366 | 4.79336 | | |
| | 5 | 0.04351 | 0.04348 | 2.49143 | | | 0.08126 | 0.08108 | 4.64539 | | |
| | 1 | -0.0078 | -0.0078 | -0.4453 | | | 0.22766 | 0.22385 | 12.8256 | | |
| | 2 | 0.05014 | 0.0501 | 2.87062 | | | 0.18604 | 0.18394 | 10.5387 | | |
| 11 | 3 | -0.037 | -0.037 | -2.1189 | 1.8548 | 0.3479 | 0.19371 | 0.19134 | 10.9631 | 1.1699 | -10.64 |
| | 4 | 0.01949 | 0.01949 | 1.11677 | | | 0.21459 | 0.21139 | 12.1115 | | |
| | 5 | 0.0003 | 0.0003 | 0.0171 | | | 0.17559 | 0.17382 | 9.95919 | | |
| 12 | 1 | 0.11124 | 0.11078 | 6.34746 | 2 2222 | 0 1656 | 0.05187 | 0.05182 | 2.96911 | 0 9875 | -1 045 |
| Τζ | 2 | -0.012 | -0.012 | -0.6859 | 3.2233 | -0.1050 | 0.02779 | 0.02778 | 1.59177 | 0.3075 | -1.045 |



| | 3 | -0.0175 | -0.0175 | -1.0004 | | | 0.01167 | 0.01167 | 0.66864 | | |
|----|---|---------|---------|---------|--------|---------|---------|---------|---------|--------|--------|
| | 4 | -0.0263 | -0.0263 | -1.5091 | | | 0.01424 | 0.01424 | 0.81565 | | |
| | 5 | 0.01493 | 0.01493 | 0.85552 | | | 0.04119 | 0.04117 | 2.35879 | | |
| | 1 | -0.2041 | -0.2014 | -11.538 | | | -0.1515 | -0.1504 | -8.6172 | | |
| | 2 | -0.2344 | -0.2303 | -13.193 | | | -0.1382 | -0.1373 | -7.8672 | | |
| 13 | 3 | -0.248 | -0.2431 | -13.926 | 1.7782 | 14.6152 | -0.1664 | -0.1649 | -9.4498 | 0.9066 | 9.5781 |
| | 4 | -0.2686 | -0.2624 | -15.034 | | | -0.1505 | -0.1494 | -8.5609 | | |
| | 5 | -0.2906 | -0.2828 | -16.205 | | | -0.1802 | -0.1783 | -10.216 | | |
| | 1 | -0.3337 | -0.3221 | -18.456 | | | -0.0767 | -0.0765 | -4.3851 | | |
| | 2 | -0.4355 | -0.4107 | -23.531 | | | -0.0906 | -0.0904 | -5.1785 | | |
| 14 | 3 | -0.3101 | -0.3007 | -17.228 | 2.9846 | 19.4249 | -0.065 | -0.0649 | -3.7173 | 0.6040 | 4.9434 |
| | 4 | -0.2784 | -0.2715 | -15.557 | | | -0.0656 | -0.0655 | -3.7529 | | |
| | 5 | -0.3477 | -0.3346 | -19.172 | | | -0.0788 | -0.0786 | -4.5038 | | |
| | 1 | -0.1359 | -0.135 | -7.7364 | | | 0.0467 | 0.04667 | 2.67387 | | |
| | 2 | -0.1646 | -0.1631 | -9.3459 | | | 0.05089 | 0.05085 | 2.91354 | | |
| 15 | 3 | -0.0792 | -0.079 | -4.5282 | 2.5216 | 8.1849 | 0.02616 | 0.02615 | 1.49849 | 0.7318 | -1.698 |
| | 4 | -0.1866 | -0.1844 | -10.568 | | | 0.05233 | 0.05228 | 2.99539 | | |
| | 5 | -0.0975 | -0.0972 | -5.5665 | | | 0.02774 | 0.02773 | 1.58882 | | |

*, These are the value obtained by adding the angle formed by the Reference articulator and the Y-axis(Supplementary Table 8) to the measured mean θ value.; SD, Standard deviation; θ , angle of the occlusal plane.



ABSTRACT (KOREAN)

안궁 이전을 통한 전통적 모형 부착법과 콘빔형 전산화 단층 영상에 기반한 가상 모형 부착법의 반복 재현성 비교 평가

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김 수 진

치과 영역에 디지털 기술이 도입되면서 많은 부분들이 전통적인 방법에서 디지 털 기법으로 대체되고 있으나 가상 모형을 가상 교합기로 위치시키는 과정에서 난관에 봉착하게 된다. 환자의 위치 정보를 가상 교합기로 옮기기 위해서는 실제 환자에서 안궁 이전을 시행하여 전통적인 방법으로 교합기에 모형을 부착한 뒤 이를 탁상형 스캐너로 스캔 하여 가상 교합기로 옮겨야 하는데 이러한 과정 자체 가 번거롭고 복잡하다. 이러한 단점을 해소하고자 가상 모형을 가상 교합기로 옮 기기 위한 많은 기법들이 소개되었으나 아직까지 명쾌한 방법은 채택되지 않았고, 주로 임의로 위치시키는 경우가 많은 실정이다.

이에 본 연구에서는 콘빔형 전산화 단층 영상의 관측 시야가 넓은 경우 두경부 해부학적 구조들 간의 위치정보를 얻을 수 있음에 착안하여 콘빔형 전산화 단층

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영상을 활용한 디지털화된 안궁 이전 기법을 소개하고, 콘빔형 전산화 단층 영상 기반의 가상 안궁을 이용한 가상 모형 부착법과 실물 안궁을 이용한 전통적인 모 형 부착법의 정확도 (precision)를 비교하고자 한다. 본 연구의 귀무 가설은 "콘 빔형 전산화 단층 영상 기반의 가상 모형 부착법과 실물 안궁을 이용한 전통적인 모형 부착법 간의 정확도 차이는 없다." 이다.

실험군은 전통적인 모형 부착 그룹 (CM)과, 가상 모형 부착 그룹 (VM) 두 군 으로 나뉜다. 두 군을 비교할 때 기준점으로 사용할 반조절성 교합기 (Hanau Modular Articulator System, Whip Mix Corp., Louisville, KY, USA)를 산업용 스캐너로 스캔하여 기준 교합기를 제작한다. CM은 실물 안궁을 이용하여 교합기 에 모형을 부착 한 뒤 산업용 스캐너를 이용하여 교합기 전체를 스캔해 기준 교 합기와 같은 위치로 정합시킨다. VM은 환자의 콘빔형 전산화 단층 영상 영상을 캐드 소프트웨어 (Exocad cad software, ExocadGmbH, Germany) 상에서 두개 골 모형 (STL format)으로 변환하고 안궁을 교합기에 장착한 상태로 산업용 스 캐너로 스캔한 가상 안궁을 이용해 두개골 모형을 기준 교합기에 위치시킨다. 두 그룹 모두 중첩의 매개체를 이용해 하나의 대표 모델을 기준 교합기상으로 위치 시킨다. 그 뒤 역설계 소프트웨어 (Geomagic Control X, 3D Systems, South Carolina, USA) 상에서 #11, 16, 26 치아에 표적 지점을 설정하고, 3차원 공간좌 표에서의 X, Y, Z 좌표값을 구한다.

CM과 VM간의 차이점을 분석하기 위해 표적 지점간의 평균 거리, 각 축별로 측 정한 표준편차, #11 치아에서 X, Y, Z축에 대한 기법 별 위치관계, 교합 평면의

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각도라는 4가지 측면에서 비교분석 하였다. 정규성을 평가하기 위하여 Kolmogorov-Smirnov test를 수행하였고, 정규성을 따르는 경우 paired t-test, 그렇지 않은 경우 Wilcoxon signed rank test 수행하였다.

설정한 표적 지점간의 평균 거리는 전통적인 기법이 가상 기법에 비해 유의하 게 큰 결과를 보였다 (P<0.01). 또한 좌표점들 사이의 표준편차도 전통적인 기법 이 가상 기법에 비해 더 크게 측정되었다 (P<0.05). 전통적인 기법에서는 다른 축들에 비해서 Z축 (상하) 방향의 표준편차가 특히 높은 경향을 보였다. #11번 치아에서 가상 기법의 경우 전통적인 기법에 비해 더욱 전방으로 위치하였으며 (P<0.01) 5번의 반복 횟수 중 1번의 경우에서 (20%) 전통적인 기법이 가상 기 법에 비해 더 상방으로 위치하는 경향을 보였다 (P<0.05). 교합 평면의 각도는 전통적인 기법이 더 유의하게 컸다 (P<0.001).

분석한 네 가지 방법으로 인해 본 연구의 귀무 가설은 기각되었으며 가상 기법 이 전통적인 기법에 비해 더 높은 정확도 (precision)를 보이는 것으로 판명되었 다. 향후 임상적인 유용성을 검증하기 위해 추가적인 연구가 필요할 것이다.

핵심 되는 말: 가상 교합기, 가상 마운팅 기법, 가상 페이스 보우, 고전적인 방법 의 마운팅과 가상 마운팅의 비교, 디지텉 치의학, 직접 디지털법, 콘빔형 전산화 단층 영상 기반의 가상 마운팅,

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