

**(DAF)**  
**(SEDAF)**

( )

( )

**2000 6**





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D.A.F : Dissolved air flotation

SE DAF : Sedimentation dissolved air flotation

THM : Trihalomethane

TOC : Total organic carbon

NTU : Nephelometric turbidity unit

CGS : Conventional gravity settling

PAC : Poly aluminum chloride

가  
 가 .  
 (Sand filtration)  
 (algae bloom) 가 가  
 가  
 (DBPs)  
 DAF system  
 가 Pilot test  
 DAF system 가  
 . ( )1  
 6,000 DAF system 1 7,200 DAF  
 system DAF system

1. DAF system

DAF system , ,가 (saturator) (Flotation chamber) 가 Henry 1.7-4.9kg/cm<sup>2</sup>

가 .

## 2. DAF system

1997 10 1 6,000 DAF  
system 98 7 7,200 / DAF system

DAF system

Plant 가  
가 .

3. . , ,

chloropil-a, TOC, UV-254, , KMnO

, Fe, Mn, Cu, Zn, NO<sup>-</sup>N, DAF system

4 . DAF system (slow sand filtra)  
4.5 , 1

5. , BOD

(algae bloom) ,

가 ,

(DBPs)

가  
가 가 C

가 .

•

290 / 57% 164

( ,1997).

,

가 ,

가 가

가

( ,1998).

DAF System 가

,

가

PILOT test

DAF system

가 , 1997

(

) 1 6,000

DAF system 1 7,200

SE DAF system

plant

DAF

system

.

•

DAF System 가 ,  
 가  
 PILOT test

DAF system  
 . 1997 ( )  
 ) 1 6,000 DAF system 1  
 7,200 SE DAF system  
 DAF system  
 plant DAF system

## 1. DAF system

DAF system , 가 (saturator)  
 (Flotation chamber) 가 . Henry  
 가 가

( ,1980). system  
 1.7-4.9 kg/ cm<sup>2</sup> 가 0.5-3.0 가  
 ( ,1995). 가 가

40 $\mu$ m

가 . 가

,

가

가

가

. ,

가

가

가 floc .

DAF가 ( ,1996).

가 가 가 가

(total flow pressurization), 가 (partial flow pressurization)

가 (recycle flow pressurization) ,

가

가

## 2. DAF

90 .

( ,1998).

가 floc

가

(

,1998).

가

가

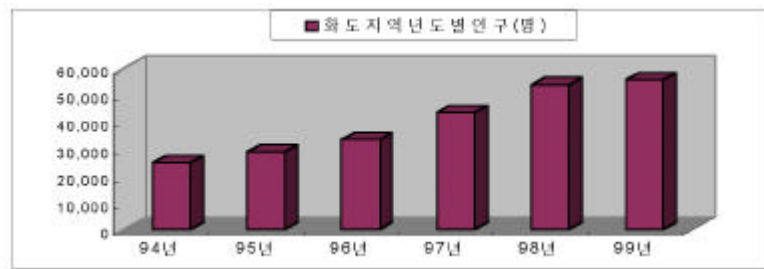
DAF

H 3,830 1 2 270 1 4,800

89

H 3,000

97



1. 가 ( ,94-99)

1 55,000 / 97 3 , 2000

2

6

가

10

6,000 /

가 ,  
 , 가 DAF  
 DAF  
 .( ,1999)  
 DAF system  
 SEDAF system  
 1 7,200 가 ( ,1998).

3.

DAF system 가  
 DAF system SEDAF  
 system plant 가  
 , 1 6,000 DAF  
 system 1 7,200 SEDAF system  
 , 1 7,200 SEDAF  
 system  
 가 가  
 가 .



•

1.

가.

가

PLANT

DAF

PILOT

SE DAF system

DAF system

1990 4,800 /

97 1

( 7,200 / )

97 10 DAF system 6,000 / , 98 7

SE DAF system ,

DAF system

97 1 97 9

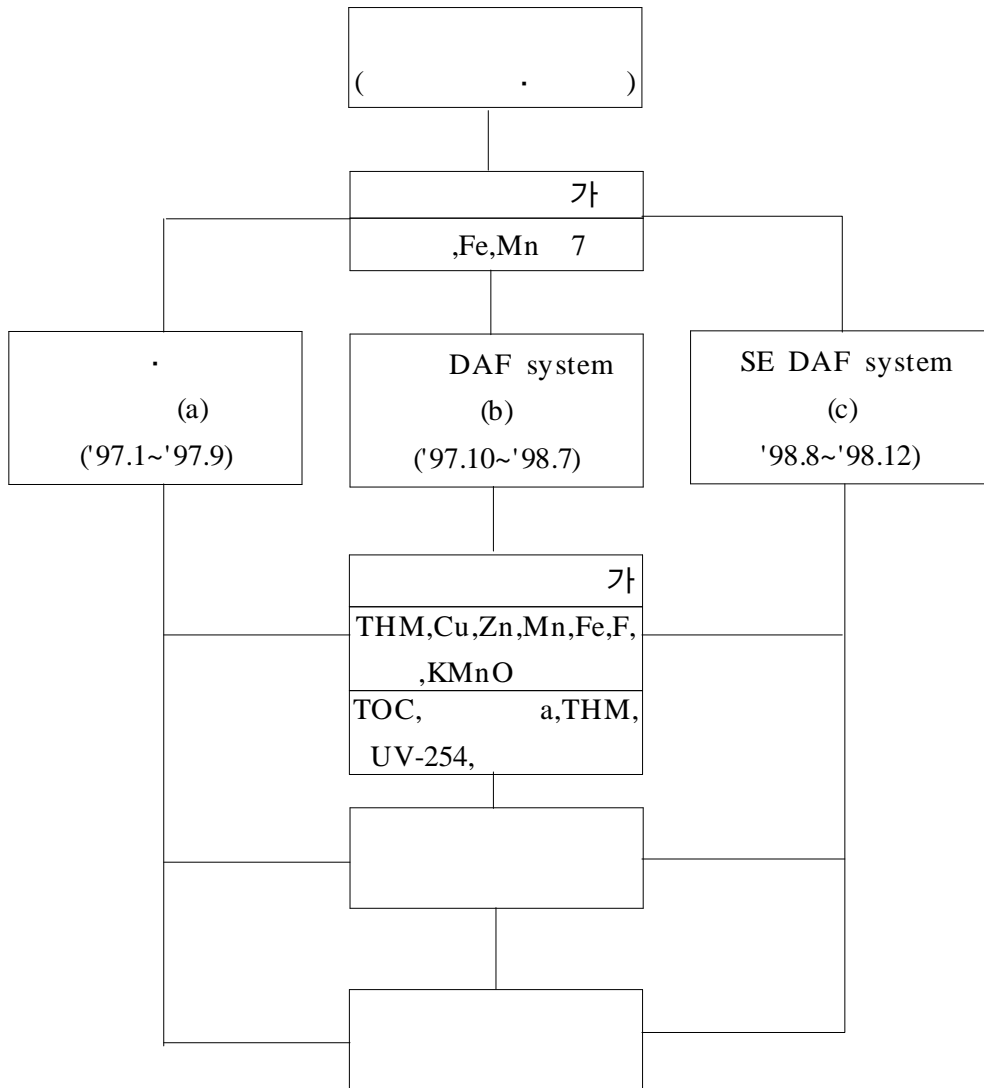
a,

DAF

SE DAF

b, SEDAF

c .



2.

PILOT

PLANT

가 97 9 a , DAF system 97

2 97 10 98 7 SE

b , SEDAF

system 98 8 98 12

c .

. 97 1 98 12

. , PAC 10~50 PPM

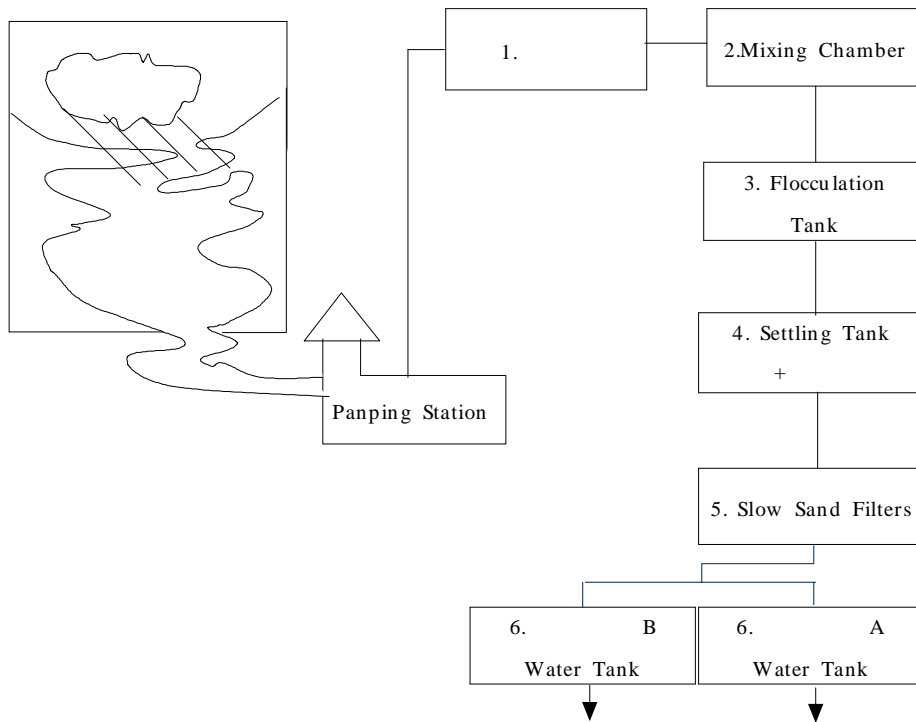
. 30%

. , 가 3.5~4.5kg/ cm<sup>2</sup> ,

. ,

0.2-1.2 PPM .

(a,b,c) .



2. a. ( )

1.  $35.8\text{m}^3$  ( 2m, 6.4m, 2.8m)

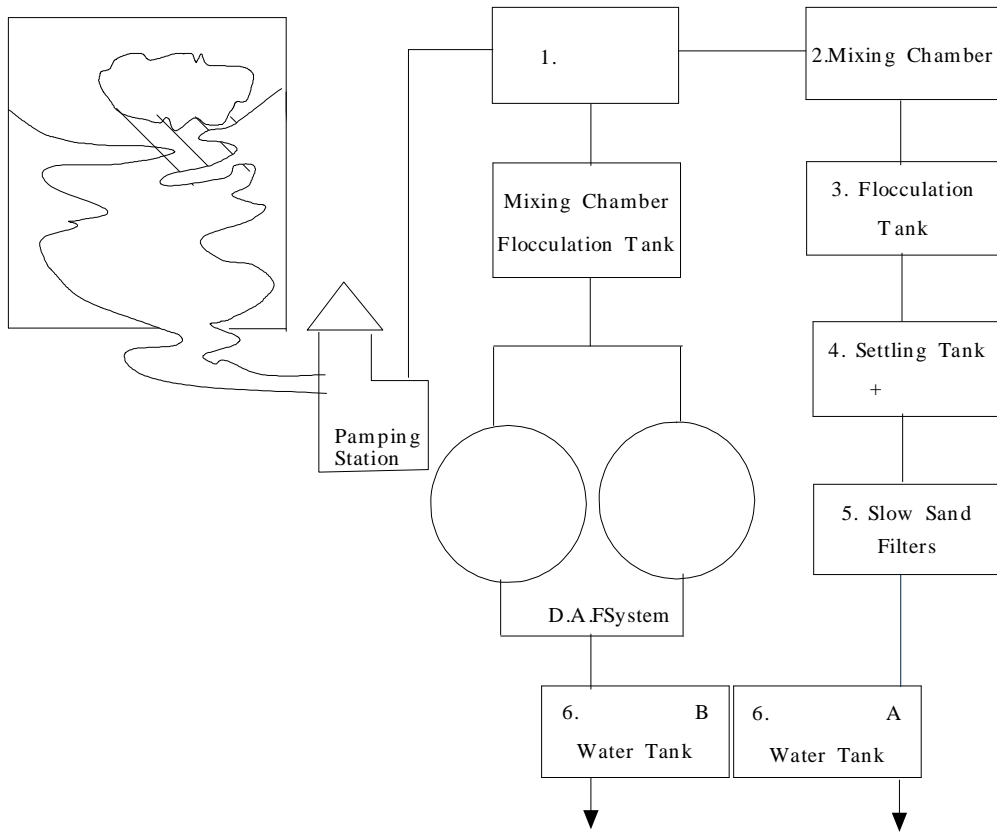
2.  $12.5\text{m}^3$  ( 2.5m, 2.5m, 2m)

3.  $50\text{m}^3$  ( 5m, 5m, 2m, 2 )

4.  $450\text{m}^3$  ( 5m, 30m, 3m, 2 )

5.  $995\text{m}^2$  (15.8m, 21m, 3 )

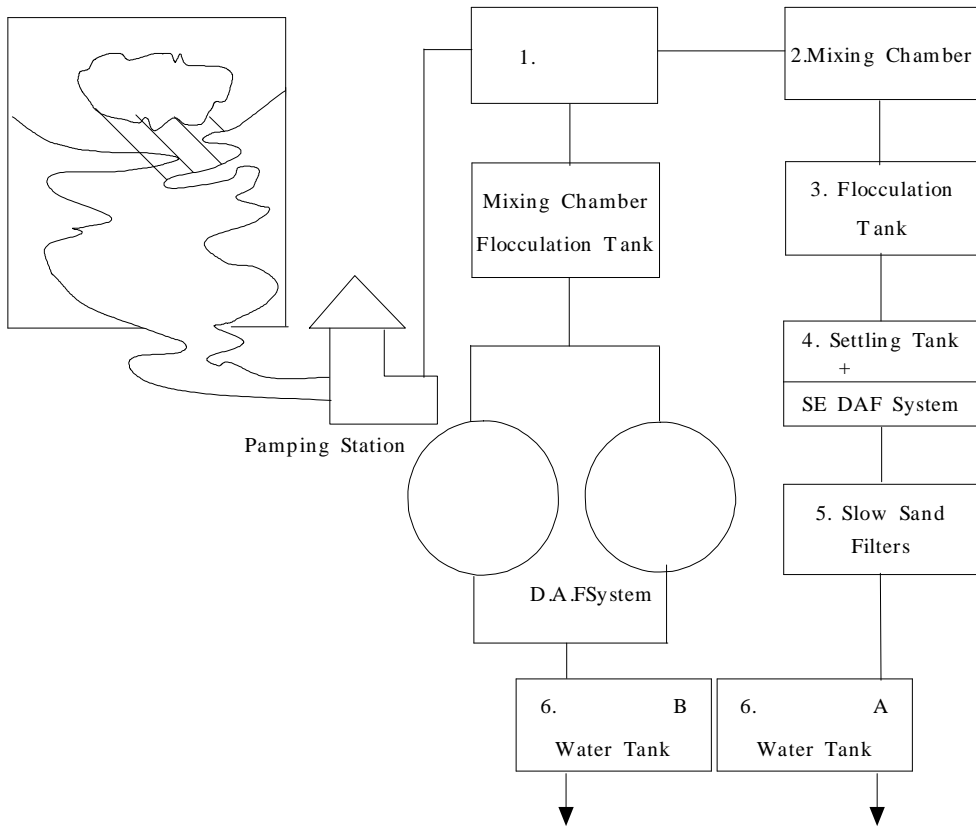
6.  $1600\text{m}^3$  ( 16.8m, 16.8m, 3m, 2 )



3. b.

DAF system

DAF SYSTEM 1	6,000	97	10
(7,200 / )		(97.10~'98.7)	(b)



4. c ( DAF system SE DAF )

가.

(1)

97 1  
98 12 9 HACH DR-2000

(2)

1~3

가

a, b, c

(c)

(1)

b Type(

) 97 10 98 5 1~3

DAF system

SE DAF system

c Type

'98. 7~12 1~2 .

, THM, -a, UV-254, TOC, KMnO ,  
, F, Fe, Mn, Cu, Zn ,

(2)

a, b, c

1 a, b, c

43 ND

1

2. a type : (7,200 / ) '97. 1

'97. 9 , ,

3. b type : '97.10~'98.7 (7,200 / ) DAF  
(6,000 / ) DAF (6,000 / )

3. c type : '98.8~'98.12 DAF(6,000 / ) a type

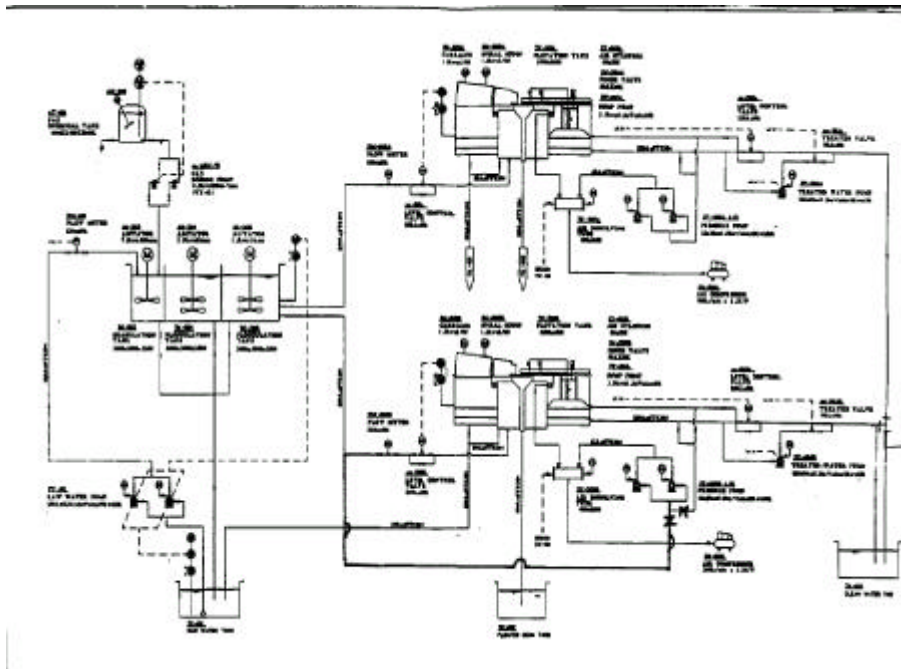
SE DAF(7,200 / ) SEDAF system



. DAF

DAF

, 가 ,



5. DAF

**. DAF system**

(Q) :  $125\text{m}^3/\text{hr}$  ( $3,000\text{m}^3/\text{day}$ , 1set )

(SS) : 5 PPM

(T) : 5~15 min

(S.L) :  $6.6\sim 9\text{m}^3/\text{m}^2 \cdot \text{hr}$

(H) : 0.9 m

가 TUBE

(T) : 9~20 sec

(SS) : 5 PPM

(Rr) :  $Q_r / Q_o$

: 15~40%

(1) DAF

:  $2.35\text{m}^2 + 21.13\text{m}^2 = 23.48\text{m}^2$

(D) : 5.5 m

(V) :  $21.4 \text{ m}^3$

(T) :  $T = V / Q = 21.4 / (125+37.5) \times 1 / 60 = 7.90 \text{ min}$

( ) :  $SL = Q / A = 125+37.5 / 21.13 = 7.69\text{m}^3/\text{m}^2 \cdot \text{hr}$

가 TUBE

$$(Q_r) : Q_o \times R_r = 125\text{m}^3/\text{hr} \times 0.3 = 37.5\text{m}^3/\text{hr}$$

SS  $R_r = 30\%$  ( 가 )

Bencl scale ADT  $4.5\text{kg}/\text{cm}^2$  (Recyle Ratio) 30%  
97.7% .

Total

:  $\varnothing 1.828\text{m}$ ,  $\varnothing 5.5\text{m}$  1m

가 :  $\varnothing 0.4\text{m} \times 1.6\text{m}$

$$: 2\text{m} \times 3\text{m} \times 3.5\text{m} = 21\text{m}^3$$

$$1 \quad 3\text{m} \times 3\text{m} \times 3.5\text{m} = 31.5\text{m}^3$$

$$2 \quad 3\text{m} \times 3\text{m} \times 3.5\text{m} = 31.5\text{m}^3$$

$$21 + 31.5 + 31.5 = 84\text{m}^3$$

(2) SE DAF system 1set

(Q) :  $150\text{m}^3/\text{hr}$  ( $3,600\text{m}^3/\text{day}$ , 1set )

(SS) : 5 PPM

$$(T) : V/Q = 30\text{m}^2 / (150+45) \times 1 / 60 = 9.23 \text{ min}$$

$$(S.L) : Q/A = 150+45 / 30 = 6.5\text{m}^3 / \text{m}^2 \cdot \text{hr}$$

(H) : 3.0 m

$$(A) : 5\text{m} \times 6\text{m} = 30\text{m}^2$$

$$(V) : A \times H = 30\text{m}^2 \times 3\text{m} = 90 \text{ m}^3$$

가 TUBE (Qr) :  $Q_o \times R_r = 150\text{m}^3/\text{hr} \times 0.3 = 45\text{m}^3/\text{hr}$

SS Rr = 30% ( 가 )

가 TUBE :  $\varnothing 0.4\text{m} \times 1.92\text{m}$

: ( )

$2\text{m} \times 3\text{m} \times 2\text{m} = 12\text{m}^3 \times 1 = 12\text{m}^3$

$5\text{m} \times 5\text{m} \times 2\text{m} = 50\text{m}^3 \times 2 = 100\text{m}^3$

.

1. : (4,800 / )

: 612

: D= 700mm L= 40.0m

: D=3.0m H=10m 1 L.W.L+17.78m,

EL+16.1m

: 3 Q=1.83m<sup>3</sup>

/ min, H= 130m,100HP

: 1 ( 6.6m, 9.6m 10m)

2.

: D= 350mm, L=7,130m

3.

: 1 ( 2m, 6.4m, 2.0m)

35.8m,

:9.7 ( 1.5 )

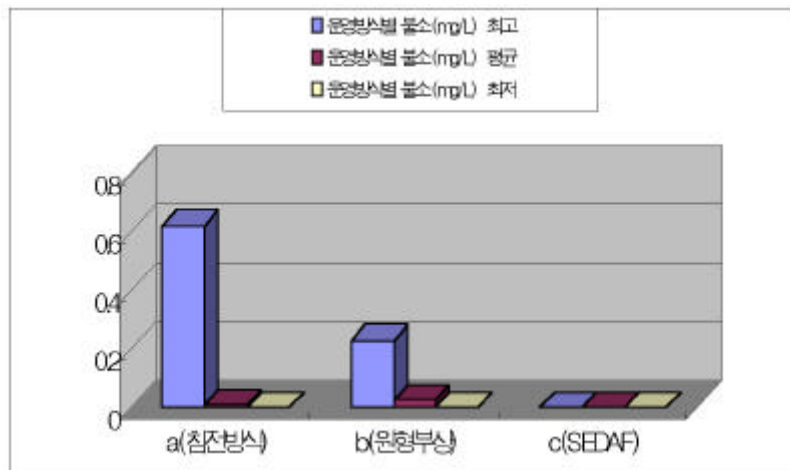
: H.W.L 2.0m  
 : 1 ( 2.5m, 2.5m, 2.0m)  
 12.5m<sup>3</sup>  
 3.3 ( 1~5 )  
 : H.W.L +131.65m  
 : , 2HP 1  
 : 2 ( 5m, 5m, 5m)  
 50m<sup>3</sup>  
 : 27 ( 20~40 )  
 : H.W.L +131.37m  
 : 3HP 4  
 : 900m<sup>3</sup> ( 5m, 30m, 3m, 2 )  
 4.1 ( 3~5 )  
 : 1:6 ( 1:3 ~ 1:8)  
 : 1.73m, 1m, 250 2 60 (97 1 )  
 :( 15.8m, 21m, 3 )  
 : PAC 50L/ hr  
 : 15m<sup>3</sup> 1  
 : 7kg/ hr, 2  
 ( ) : 16.8m, 16.8m, 3m × 2  
 800m<sup>3</sup> ( 1,600m<sup>3</sup> )  
 :H.W.L+ 126.76m, L.W.L+123.76m ( , 1995)

1.

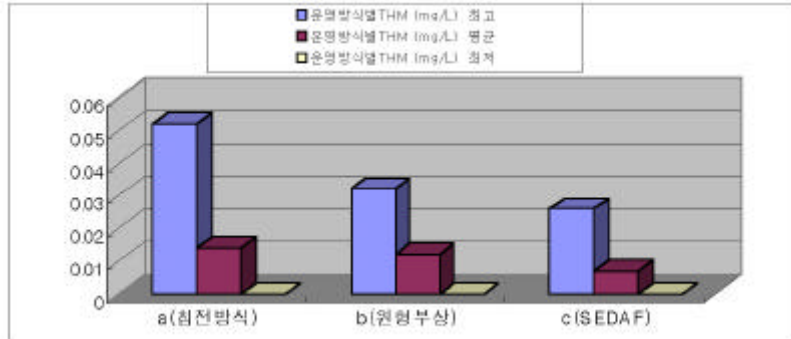
- (a), (97.1 - 97.9)
- (b), DAF (97.10 - 98.7)
- (c), SEDAF (98.8 - 98.12)

(a), (b), (c),

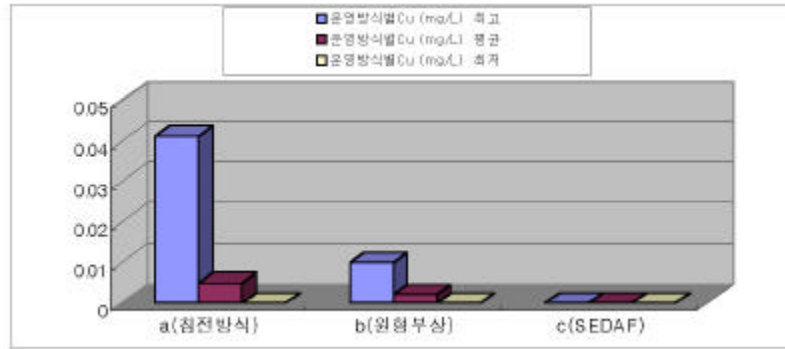
, SEDAF (c)가 가  
 가 , (b) DAF 가 (a)type  
 가 .



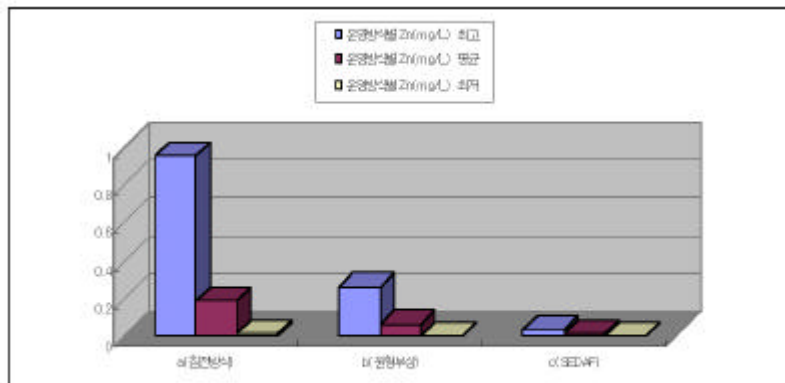
6. a,b,c



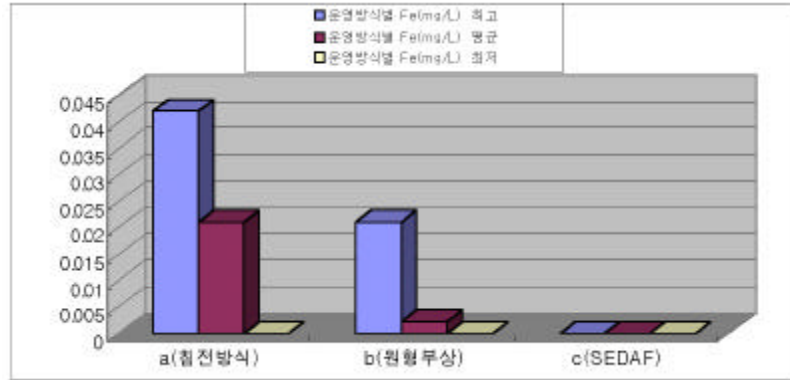
7. a,b,c THM



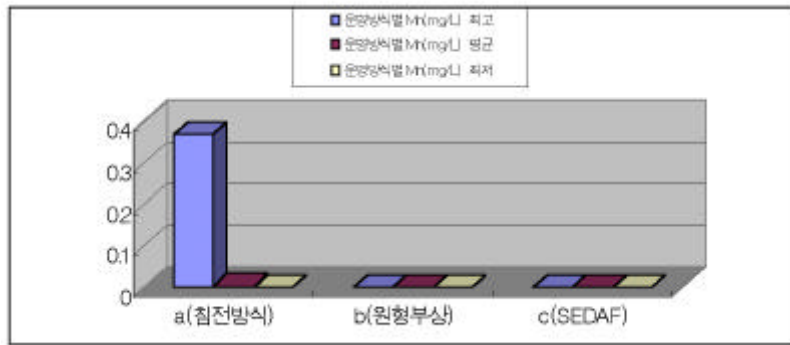
8. a,b,c Cu (mg/l)



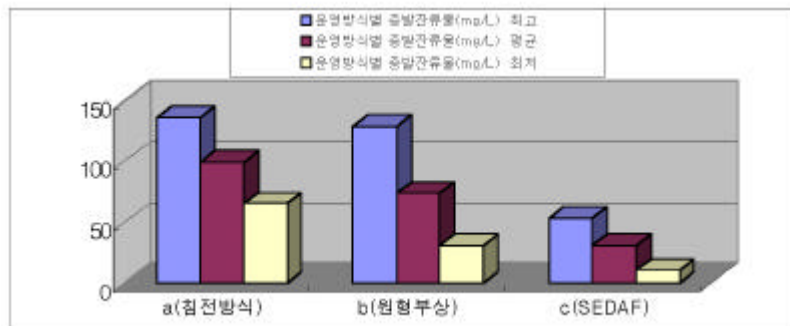
9. a,b,c Zn (mg/l)



10. a,b,c Fe (mg/l)

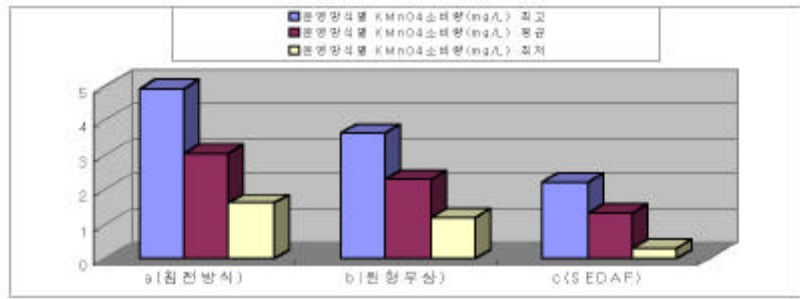


11. a,b,c Mn



12. a,b,c





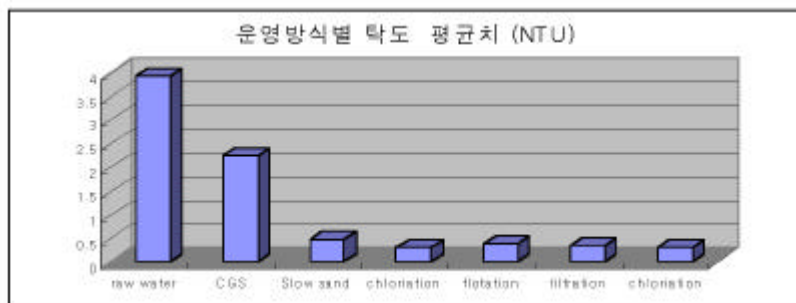
13. a,b,c KMnO (mg/l)

DAF system 가 Fe, Mn, Cu, Zn,

가

2.

a,b



14. a,b Type (NTU)

88.3%

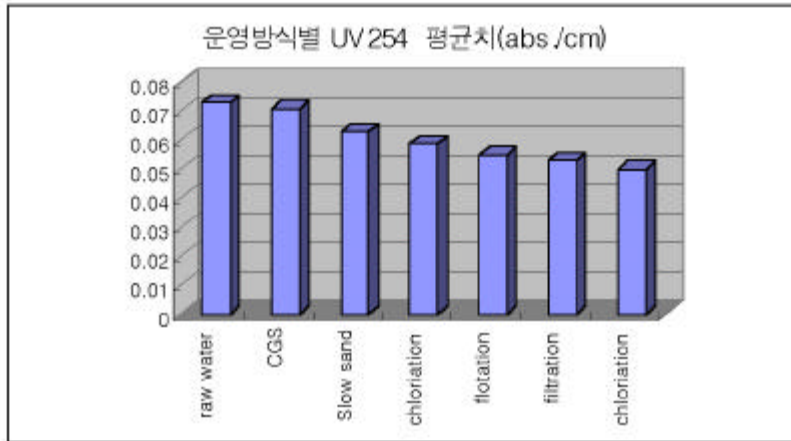
43%

45.3%

DAF

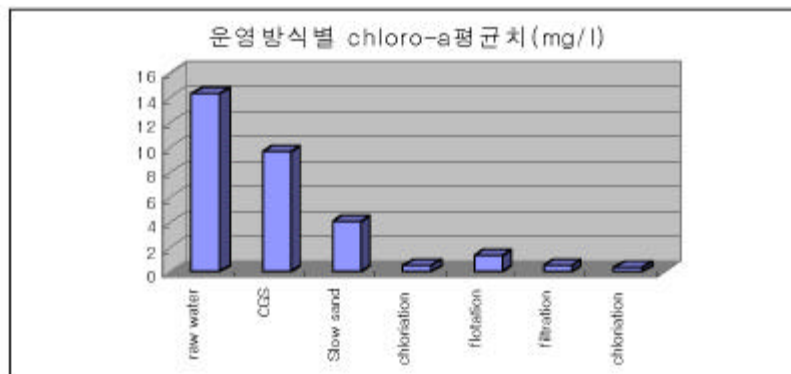
89%

가 가



15. a,b Type UV254 (abs./cm)

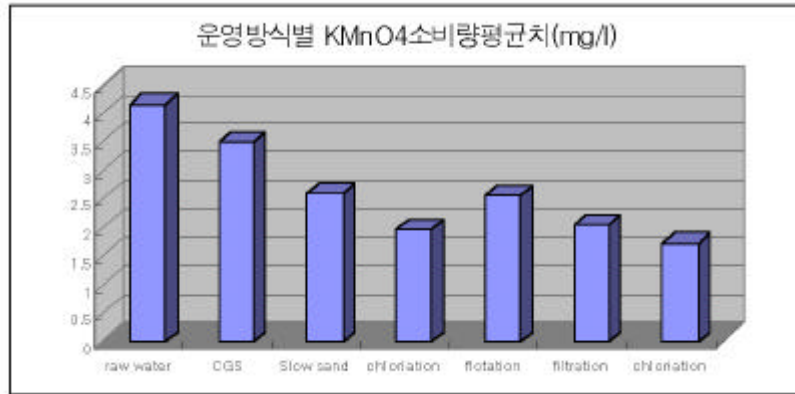
UV-254



16. a,b Type -a (mg/ m<sup>3</sup>)

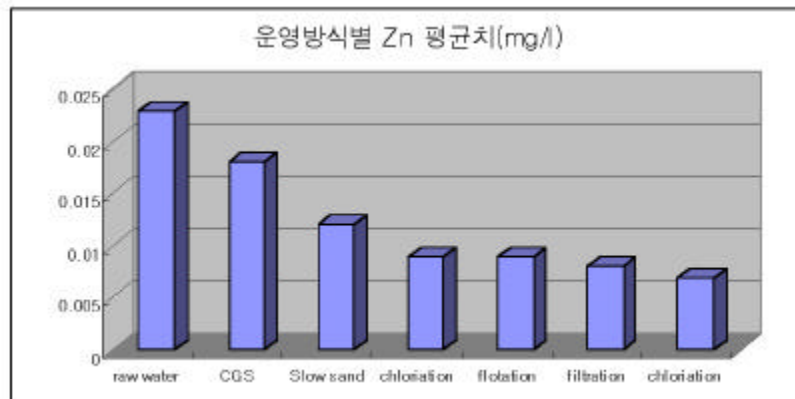
-a 32% 91%

-a 가



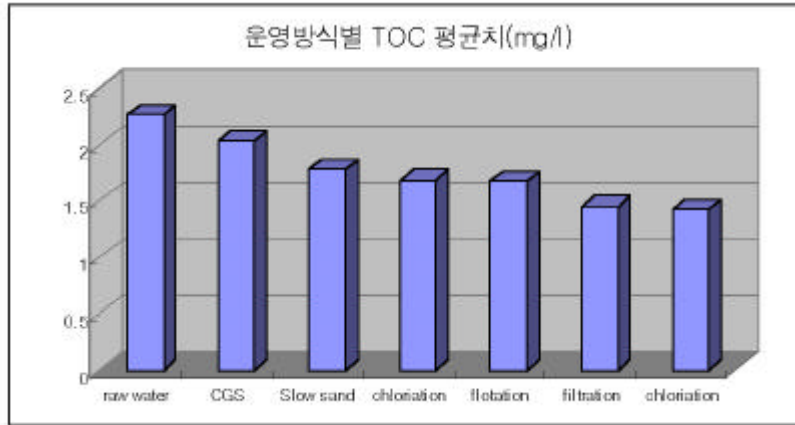
17. a,b Type KMnO

KMnO 16%, 41% , 2.5



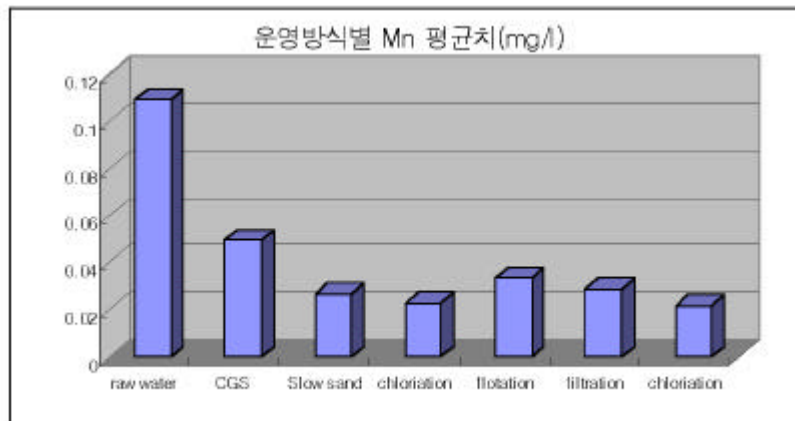
18. a,b Type Zn

22%, 65% 3



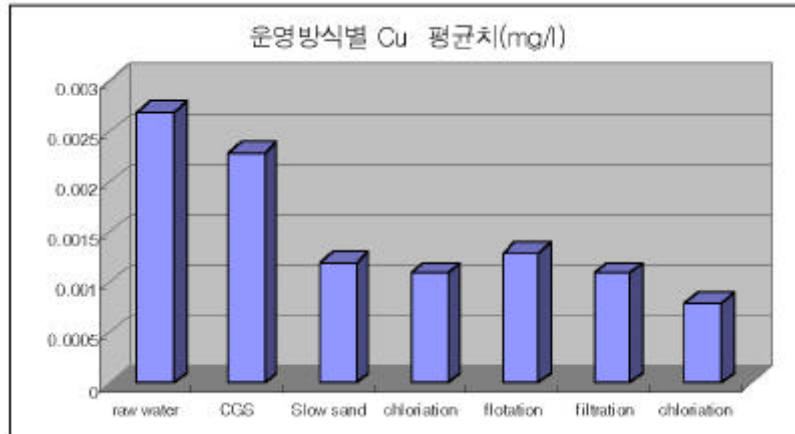
19. a,b Type TOC

TOC 17%, 33% 2



20. a,b Type Mn

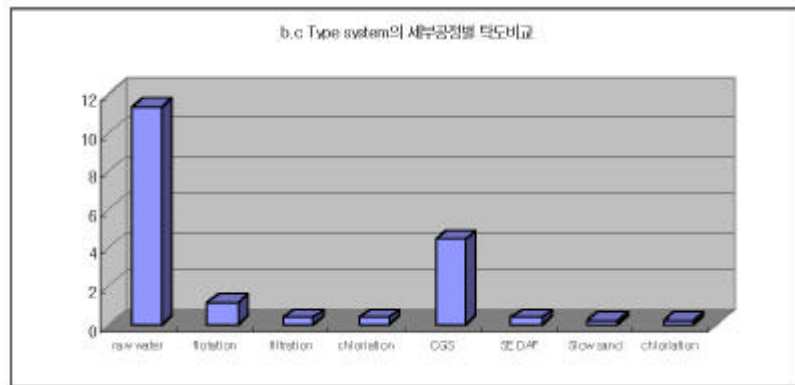
56%, 67%



21. a,b Type Cu

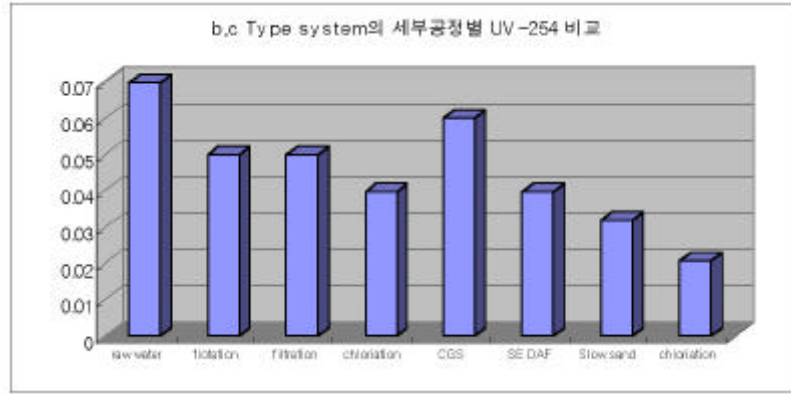
15%, 48% 3

b,c Type



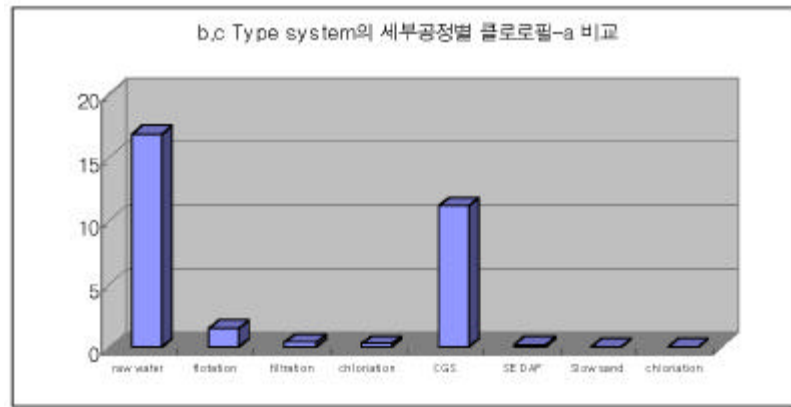
22. b,c Type

DAF(b) 97%, SEDAF(c) 99%



23. b,c Type UV-254

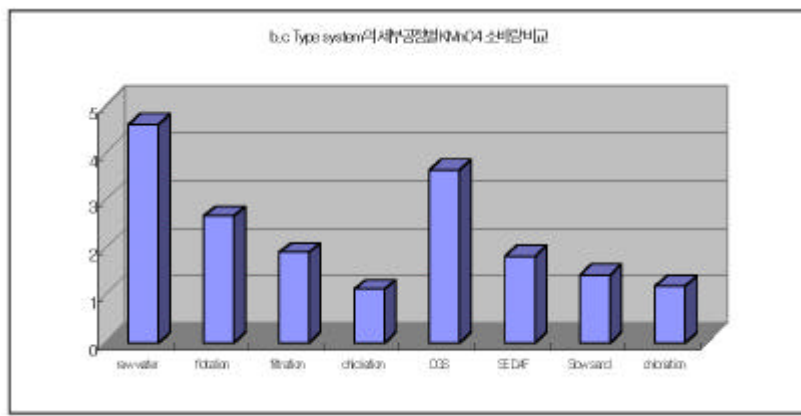
UV-254 DAF(b) 43%, SEDAF(c) 70%



24. b,c Type a

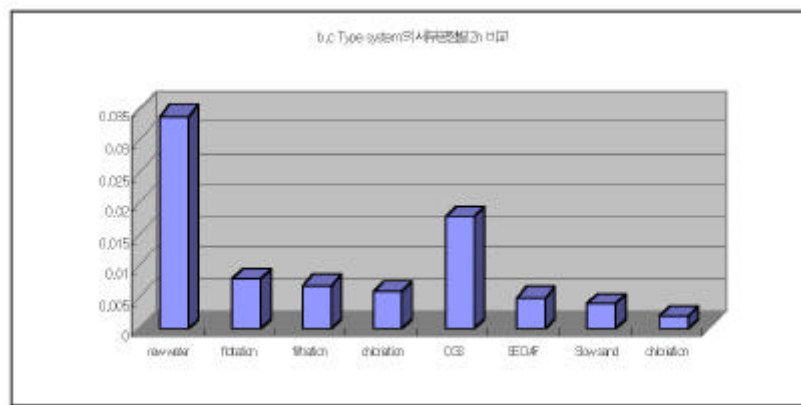
a DAF(b) 98.6%, SEDAF(c) 99.7%

SEDAF 가



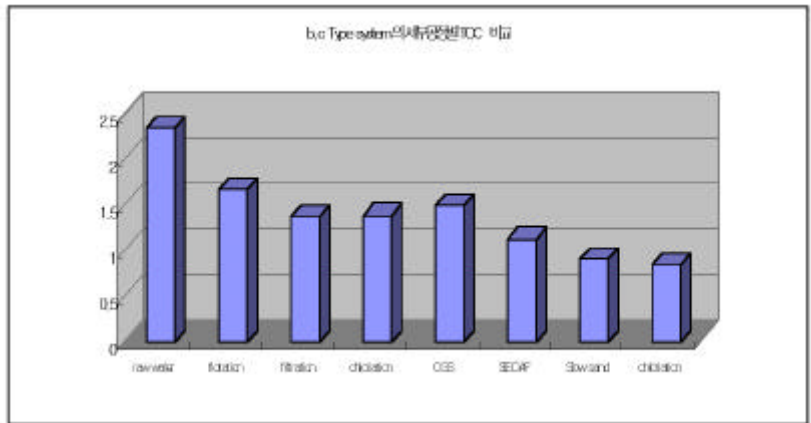
25. b,c Type KMnO

KMnO DAF(b) 60.5%, SEDAF(c) 74.5%  
 SE DAF 가 .



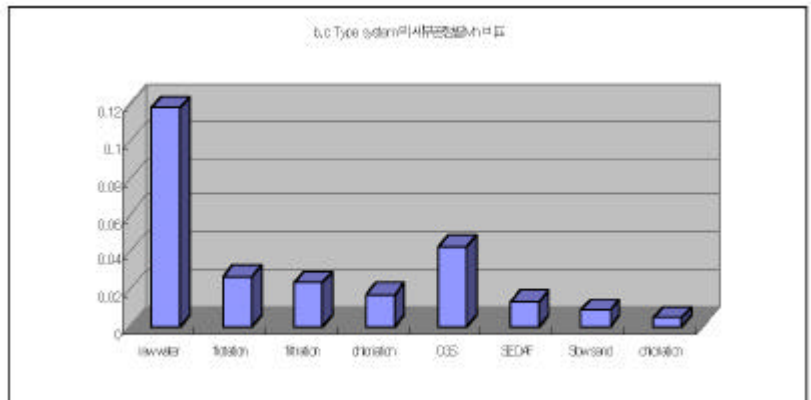
26. b,c Type Zn

Zn DAF(b) 76.5%, SEDAF(c) 94.1% .



27. b,c Type TOC

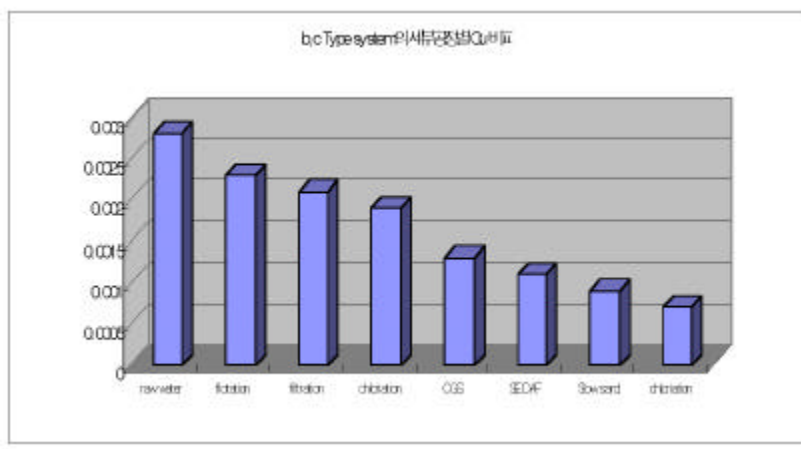
TOC DAF(b) 40.7%, SEDAF(c) 63.9%



28. b,c Type Mn

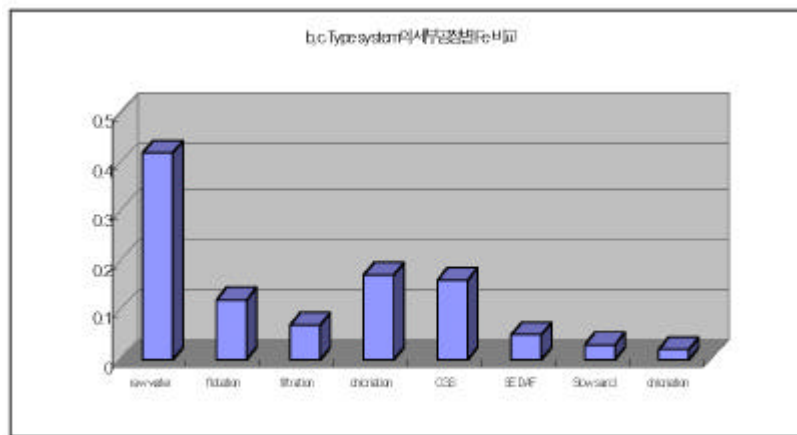
Mn DAF(b) 85.2%, SEDAF(c) 95.8%





29. b,c Type Cu

Cu DAF(b) 32.1%, SEDAF(c) 75% 2



30. b,c Type Fe

Fe DAF(b) 59.5%, SEDAF(c) 95.2%

.

# 1. DAF system

DAF system

$$: 2.35\text{m}^2 + 21.13\text{m}^2 = 23.48\text{m}^2 \times 2 = 46.96\text{m}^2$$

$$23.48\text{m}^2 \times 2 = 46.96\text{m}^2$$

$$: 6,000\text{m}^3 / 46.96\text{m}^2 = 128\text{m}$$

$$: 21.13\text{m}^2 \times 2 = 42.26$$

, 46.96m<sup>2</sup>

.

$$: 5\text{m} \times 30\text{m} \times 2 = 300\text{m}^2$$

$$: 15.8\text{m} \times 21\text{m} \times 3 = 995.5\text{m}^2$$

$$995.5\text{m}^2 + 300\text{m}^2 = 1295.5\text{m}^2$$

CGS/ DAF

$$1295.5\text{m}^2 / 46.96\text{m}^2 = 28$$

1/ 28

가

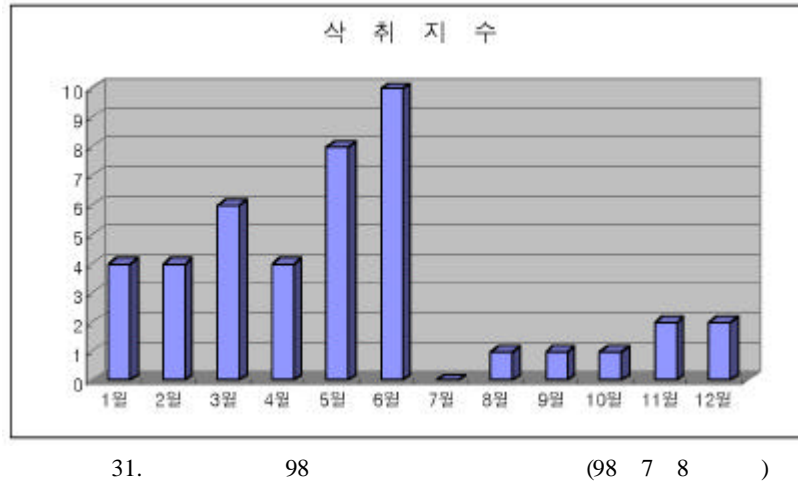
:

,

28:1

.

## 2. SE DAF system



SEDAF                  6                  36 ,                  7

3 / 1

21 ~2 / 1

1

$$15.8\text{m} \times 21\text{m} \times 0.08\text{m} \times 2 = 53\text{m}^3$$

$$53\text{m}^3 \quad 177$$

$$1,770,000 \times 72 / = 127,440,000$$

$$1,770,000 \times 14 / = 24,780,000$$

$$72 - 14 = 58$$

$$58 \times 1,770,000 = 102,660,000$$

SE DAF system = 102,000,000  
1 가 .  
가 가 DAF  
system 가 가 .

•

	DAF system	SE DAF
system	, THM, Cu, Zn, Fe, Mn,	
, KMnO	DAF system	
	DAF system	SE DAF system
	45.3%	88.3%
	89%	43%,
SE DAF	96.8%	가 가
가 0.18NTU		
UV-254		0.05 abs./ cm,
abs./ cm, SE DAF	0.021 abs./ cm	0.04
Chlorophyll-a		97.2%
	32%	, DAF
	98.4%	91%, SE DAF
	99.7%	99.1%
KMnO		16%
, DAF		41%
	61%	SE DAF

Zn 22%, DAF  
65%, SE DAF 85.3%

TOC 17% , 33%  
SE DAF 52%

Mn 56%, 67%, SE DAF  
89%

( -a,TOC, )  
SE DAF system

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1. a Type

		1997								
		1	2	3	4	5	6	7	8	9
	100CFU/ 1M $\ell$	1	0	1	13	6	3	0	0	0
		N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.05	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	1.5	N · D	N · D	N · D	N · D	0.62	N · D	N · D	N · D	N · D
	0.05	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.01	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
		N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
		N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
6가	0.05	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.5	N · D	N · D	0.14	0.06	N · D	N · D	N · D	N · D	N · D
	10	1.7	14	1.5	1.9	1.7	1.5	2.2	14	14
	0.01	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.005	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.1	0.052	N · D	N · D	0.052	N · D	N · D	N · D	N · D	0.02
	0.07	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.02	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.06	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.25	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.04	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.002	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
1.1.1	0.1	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.01	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.03	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D

2. a Type

		1997									
		1	2	3	4	5	6	7	8	9	
1.1	0.02	N · D	N · D	0.007	N · D	N · D	N · D	N · D	N · D	N · D	
	0.01	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	
	0.7	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	
	0.3	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	
	0.5	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	
	0.03	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	
	10	2.3	3.0	4.1	3.2	2.4	3.1	2.7	4.9	1.6	
	300	45	54	72	40	37	27	46.1	26.3	33	
	PH	1	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	0.041
		5	N · D	N · D	N · D	N · D	1	N · D	N · D	N · D	N · D
0.5		N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	
5.8~8.5		7.0	7.1	7.2	7.1	6.9	6.9	7.4	7.0	6.9	
1		0.209	0.145	0.01	0.132	0.114	0.019	0.021	0.951	0.092	
150		6.6	3.9	4.9	6	7	4.6	13	3.4	5	
500		105	97	99	88	80	136	106	118	65	
0.3		0.42	0.37	0.017	N · D	N · D	N · D	N · D	0.13	0.018	
0.3		0.037	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	
2											
200	6	5	6	7	8	6	15	5.6	6		
0.2	N · D	N · D	0.02	N · D	N · D	0.041	N · D	0.02	N · D		
	1/30	2/11	3/5	4/9	5/8	6/9	7/3	8/7	9/4		

3. b Type

		1997					1998				
		10	11	12	1	2	3	4	5	6	7
	100CFU/ 1Mℓ	0	0	0	0	0	6	0	2	2	4
		N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.05	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	1.5	N · D	N · D	N · D	N · D	N · D	0.23	N · D	N · D	N · D	N · D
	0.05	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.01	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
		N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
		N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
6가	0.05	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.5	N · D	N · D	N · D	0.01	0.05	0.02	0.12	N · D	N · D	N · D
	10	1.2	1.4	1.4	1.5	1.6	1.6	1.4	0.9	1.2	1.8
	0.01	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.005	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.1	N · D	0.021	0.012	0.015	N · D	0.032	N · D	N · D	0.004	0.031
	0.07	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.02	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.06	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.25	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.04	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.002	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
1.1.1	0.1	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.01	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
	0.03	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D

4. b Type

	1997			1998						
	10	11	12	1	2	3	4	5	6	7
0.02	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	0.015
0.01	N · D	N · D	0.001	0.001	N · D	0.001	N · D	N · D	N · D	0.001
0.7	N · D	0.001	0.002	0.02	N · D	0.02	0.001	N · D	N · D	0.056
0.3	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
0.5	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
1.1	0.03	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
10	2.5	1.1	1.8	2.2	2.8	3.6	3.0	1.2	2.7	1.9
300	29	58	41	44	51	43	63	73	83	50
1	N · D	N · D	N · D	N · D	N · D	N · D	0.006	N · D	0.010	N · D
5	N · D	N · D	N · D	N · D	1	N · D	N · D	N · D	N · D	N · D
0.5	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
PH	5.8~8.5	7.7	7.6	7.4	7.2	7.4	7.1	7.1	7.2	7.2
1	0.12	N · D	0.061	N · D	0.045	N · D	0.067	0.01	0.264	0.089
150	5	10	7	8	6	10	10	6	6	7
500	123	75	72	58	41	77	68	63	31	129
0.3	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	0.21
0.3	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D	N · D
2										
200	7	8	6	6	6	6	6	4	6	6
0.2	N · D	N · D	0.056	0.052	0.058	N · D	0.03	N · D	0.04	0.07
	10/2	11/5	12/5	1/5	2/9	3/6	4/3	5/8	6/10	7/6

5. c Type

		1998				
		8	9	10	11	12
	100CFU/ 1M $\emptyset$	4	0	4	0	0
		N · D	N · D	N · D	N · D	N · D
	0.05	N · D	N · D	N · D	N · D	N · D
	1.5	N · D	N · D	N · D	N · D	N · D
	0.05	N · D	N · D	N · D	N · D	N · D
	0.01	N · D	N · D	N · D	N · D	N · D
		N · D	N · D	N · D	N · D	N · D
		N · D	N · D	N · D	N · D	N · D
6가	0.05	N · D	N · D	N · D	N · D	N · D
	0.5	N · D	N · D	N · D	0.01	N · D
	10	1.2	1.4	1.6	1.4	1.6
	0.01	N · D	N · D	N · D	N · D	N · D
	0.005	N · D	N · D	N · D	N · D	N · D
	0.1	0.007	N · D	0.026	N · D	N · D
	0.07	N · D	N · D	N · D	N · D	N · D
	0.02	N · D	N · D	N · D	N · D	N · D
	0.06	N · D	N · D	N · D	N · D	N · D
	0.25	N · D	N · D	N · D	N · D	N · D
	0.04	N · D	N · D	N · D	N · D	N · D
	0.002	N · D	N · D	N · D	N · D	N · D
1.1.1	0.1	N · D	N · D	N · D	N · D	N · D
	0.01	N · D	N · D	N · D	N · D	N · D
	0.03	N · D	N · D	N · D	N · D	N · D

6. c Type

		1998				
		8	9	10	11	12
1.1	0.02	N · D	N · D	N · D	N · D	N · D
	0.01	N · D	N · D	0.001	0.001	N · D
	0.7	N · D	0.001	0.002	0.02	N · D
	0.3	N · D	N · D	N · D	N · D	N · D
	0.5	N · D	N · D	N · D	N · D	N · D
	0.03	N · D	N · D	N · D	N · D	N · D
	10	2.2	1.1	1.8	0.3	1.1
	300	63	58	84	103	98
PH	1	N · D	N · D	N · D	N · D	N · D
	5	N · D	N · D	N · D	N · D	N · D
	0.5	N · D	N · D	N · D	N · D	N · D
	5.8~8.5	6.9	7.2	7.1	7.3	7.0
	1	0.005	0.008	0.034	0.007	N · D
	150	4	10	10	8	11
	500	41	53	21	11	29
	0.3	N · D	N · D	N · D	N · D	N · D
	0.3	N · D	N · D	N · D	N · D	N · D
	2					
200	6	8	6	6	6	
0.2	N · D	N · D	0.03	N · D	0.07	
	8/12	9/8	10/16	11/10	12/2	



7. a,b type

	raw water	CGS	Slow sand chloriation	flotation	filtration	chloriation	
97-10-30	3.88	2.54	0.671	0.158	0.903	0.342	0.168
97--11-05	2.54	2.067	0.192	0.193	0.893	0.153	0.183
97-11-19	1.82	1.48	0.814	0.426	1.47	0.216	0.427
97-11-26	2.3	1.5	0.13	0.373	1.37	0.55	0.353
97-12-30	3.71	3.353	0.402	0.452	1.20	0.534	0.352
98-01-09	1.543	1.363	0.219	0.652	0.959	0.177	0.683
98-02-04	2.72	2.33	0.723	0.243	1.18	0.792	0.693
98-03-04	2.13	2.15	0.27	0.264	0.649	0.22	0.204
98-03-05	3.02	1.47	0.417	0.419	0.988	0.421	0.319
98-03-18	17.23	2.9	0.608	0.501	0.784	0.456	0.301
98-04-16	4.08	2.88	0.26	0.038	1.84	0.514	0.027
98-04-18	3.79	3.59	0.237	0.362	2.31	0.424	0.252
98-05-14	1.03	1.01	0.734	0.437	0.345	0.019	0.437
98-05-19	5.44	3.05	0.984	0.389	1.07	0.226	0.489
	3.945	2.263	0.475	0.350	1.140	0.360	0.349

8. a,b type

chloro-a

	raw water	CGS	Slow sand chloriation	flotation	filtration	chloriation	
97-10-30	1.265	1.002	1.000	0.557	0.866	0.552	0.257
97-11-19	7.02	5.01	3.12	0.37	0.642	0.36	0.17
97-11-26	6.179	3.891	2.018	0.34	0.621	0.33	0.24
97-12-30	15.108	12.167	4.856	0.39	0.442	0.38	0.20
98-01-09	15.98	13.47	3.86	0.26	3.97	0.25	0.19
98-02-04	19.12	11.24	8.23	0.978	0.04	0.974	0.478
98-03-10	28.15	23.791	4.736	0.002	7.427	0.007	0.002
98-03-18	26.69	12.276	2.878	0.767	0.847	0.766	0.467
98-04-14	16.87	14.18	2.66	0.04	0.88	0.04	0.01
98-04-16	10.189	8.978	4.803	0.452	0.223	0.450	0.442
98-04-18	9.299	4.21	3.591	0.326	0.364	0.325	0.306
98-04-30	15.513	9.338	5.327	0.442	0.037	0.441	0.142
98-05-19	10.148	4.306	2.628	0.224	0.691	0.223	0.024
	13.963	9.527	3.823	0.396	1.312	0.392	0.225

9. a,b type Fe

	raw water	CGS	Slow sand chloriation	flotation	filtration	chloriation	
97-10-30	0.335	0.21	0.071	0.077	0.083	0.079	0.077
97-11-19	0.249	0.22	0.018	0.103	0.175	0.026	0.103
97-11-26	0.151	0.078	0.019	0.056	0.151	0.026	0.056
97-12-30	0.315	0.229	0.04	0.087	0.092	0.04	0.087
98-01-09	0.195	0.074	0.016	0.874	0.057	0.033	0.874
98-02-04	0.324	0.099	0.134	0.17	0.132	0.097	0.17
98-03-10	0.5025	0.2197	0.1546	0.162	0.2249	0.1164	0.162
98-03-18	1.5803	0.2496	0.1327	0.179	0.1536	0.1949	0.179
98-04-14	0.3299	0.1252	0.0044	0.0033	0.0572	0.0023	0.0033
98-04-16	0.19386	0.1785	0.04358	0.031	0.11476	0.1001	0.031
98-04-18	0.3812	0.0675	0.0078	0.0056	0.0934	0.0027	0.0056
98-04-30	0.3517	0.0851	0.0092	0.598	0.13445	0.06988	0.598
98-05-19	0.3978	0.0293	0.0385	0.0391	0.028	0.0402	0.0391
	0.4081	0.1434	0.0529	0.1834	0.1151	0.0636	0.1834

10. a,b type Cu

	raw water	CGS	Slow sand chloriation	flotation	filtration	chloriation	
97-10-30	0.017	0.007	0.005	0.01	0.005	0.013	0.01
97-11-19	0.0017	0.0010	0.0011	0.0012	0.0018	0.001	0.0012
97-11-26	0.0003	0.0002	0.001	0.0013	0.001	0.0005	0.0013
97-12-30	0.0008	0.0006	0.0004	0.0009	0.0007	0.0006	0.0009
98-01-09	0.0008	0.0007	0.0006	0.0008	0.0004	0.0008	0.0008
98-02-04	0.0013	0.0010	0.0005	0.0009	0.0005	0.0011	0.0009
98-03-10	0.0007	0.0004	0.0008	0.0001	0.0007	0.0007	0.0011
98-03-18	0.0016	0.0006	0.0008	0.0015	0.001	0.0013	0.0015
98-04-14	0.0012	0.0012	0.0008	0.0007	0.0008	0.0008	0.0007
98-04-16	0.00278	0.00078	0.00154	0.00009	0.00162	0.0012	0.00159
98-04-18	0.0016	0.0016	0.001	0.0005	0.0003	0.0007	0.0005
98-04-30	0.00278	0.0010	0.000811	0.0014	0.0018	0.00146	0.0014
98-05-19	0.0019	0.0019	0.0017	0.0006	0.0018	0.0015	0.0016
	0.002651	0.00225	0.001235	0.001107	0.00134	0.001157	0.000707

## 11. a,b type

KMnO<sub>4</sub>

	raw water	CGS	Slow sand chloriation	flotation	filtration	chloriation	
97-10-30	2.2	2.5	2.3	0	2.2	1.6	0.2
97-11-05	1.896	3.16	2.896	0.632	2.889	1.316	0.630
97-11-19	2.528	3.16	2.244	0.632	2.239	1.632	0.622
97-11-26	2.84	2.21	1.26	1.26	1.24	1.06	1.16
98-12-30	5.372	2.844	2.108	3.792	2.102	2.076	1.902
98-01-09	3.792	4.424	4.128	1.58	4.10	3.264	1.47
98-02-04	2.1	2.3	2.15	1.1	2.149	1.6	1.91
98-03-04	7.09	6.75	5.02	3.63	5.01	4.23	3.93
98-03-05	7.78	4.67	4.52	3.321	4.49	3.94	3.821
98-03-18	7.44	5.19	3.69	2.08	3.65	2.9	2.08
98-04-16	7.34	5.43	3.99	2.723	3.96	2.89	2.723
98-04-18	3.79	3.82	0.297	0.369	0.28	0.124	0.369
98-04-30	1.9	0.95	0.8	0.851	0.796	0.4	0.851
98-05-14	1.59	1.91	1.08	2.879	1.06	0.78	0.79
98-05-19	4.63	2.93	0.96	0.96	0.89	0.56	0.96
	4.152	3.483	2.496	1.720	2.470	1.891	1.561

## 12. a,b type

## Zn

	raw water	CGS	Slow sand chloriation	flotation	filtration	chloriation	
97-10-30	0.053	0.035	0.032	0.033	0.022	0.012	0.004
97-11-05	0.01	0.0042	0.018	0.002	0.0036	0.0174	0.004
97-11-19	0.0017	0.0011	0.002	0.0029	0.0028	0.0018	0.0019
97-11-26	0.004	0.0055	0.0024	0.003	0.0058	0.0051	0.003
97-12-30	0.199	0.0033	0.016	0.019	0.0096	0.008	0.032
98-01-09	0.003	0.018	0.002	0.0038	0.003	0.002	0.0018
98-02-04	0.0074	0.0037	0.0045	0.0033	0.0032	0.0031	0.0023
98-03-10	0.0071	0.069	0.0029	0.0043	0.0040	0.0032	0.0043
98-03-18	0.006	0.0038	0.0037	0.004	0.0041	0.003	0.004
98-04-14	0.012	0.1028	0.0841	0.0371	0.0257	0.0240	0.0271
98-04-16	0.00954	0.00408	0.00323	0.0037	0.0199	0.01809	0.0037
98-04-18	0.0136	0.0047	0.0023	0.00242	0.0098	0.0093	0.00542
98-04-30	0.00668	0.00193	0.00446	0.00054	0.00282	0.00262	0.00254
98-05-19	0.0025	0.0015	0.0026	0.0017	0.0021	0.0014	0.0017
	0.023	0.018	0.012	0.008	0.008	0.007	0.006

## 13. a,b type

## TOC

	raw water	CGS	Slow sand chloriation	flotation	filtration	chloriation
97-10-30	1.534	1.44	2.259	1.783	1.356	1.783
97-11-05	3.277	2.986	1.113	1.111	1.092	0.883
97-11-19	1.243	1.168	1.191	1.117	1.064	0.986
97-12-30	2.02	1.98	2.03	1.97	1.89	1.84
98-03-04	2.77	1.94	2.14	1.82	1.8	1.75
98-03-10	2.7	1.71	1.89	1.69	1.88	1.31
	2.257	1.87	1.770	1.581	1.513	1.400

## 14. a,b type

## UV254

	raw water	CGS	Slow sand chloriation	flotation	filtration	chloriation
97-10-30	0.084	0.068	0.071	0.059	0.06	0.050
97-11-05	0.074	0.076	0.069	0.056	0.059	0.052
97-11-19	0.072	0.073	0.071	0.060	0.054	0.051
97-11-26	0.088	0.075	0.07	0.055	0.051	0.050
97-12-30	0.069	0.07	0.067	0.059	0.056	0.054
98-01-09	0.067	0.068	0.068	0.058	0.054	0.053
98-02-04	0.068	0.16	0.065	0.058	0.053	0.052
98-03-10	0.065	0.062	0.059	0.057	0.053	0.050
98-03-18	0.066	0.053	0.054	0.053	0.052	0.051
98-04-14	0.066	0.045	0.062	0.060	0.052	0.050
98-04-16	0.083	0.051	0.075	0.066	0.054	0.053
98-04-18	0.077	0.076	0.073	0.065	0.052	0.051
98-04-30	0.071	0.057	0.051	0.050	0.052	0.052
98-5-14	0.053	0.052	0.051	0.050	0.054	0.053
98-05-19	0.068	0.052	0.050	0.050	0.051	0.050
	0.071	0.069	0.063	0.057	0.053	0.051

## 15. a,b type

## Mn

	raw water	CGS	Slow sand	chloration	flotation	filtration	chloration
97-10-30	0.086	0.019	0.018	0.021	0.007	0.004	0.023
97-11-19	0.017	0.018	0.005	0.003	0.017	0.004	0.002
97-11-26	0.009	0.03	0.017	0.009	0.012	0.005	0.007
97-12-30	0.028	0.024	0.005	0.012	0.014	0.02	0.012
98-01-09	0.03	0.032	0.0152	0.024	0.019	0.023	0.024
98-02-04	0.083	0.081	0.0301	0.037	0.043	0.054	0.037
98-03-10	0.035	0.0341	0.0312	0.0291	0.0324	0.02	0.0291
98-03-18	0.6062	0.0074	0.0013	0.0165	0.0398	0.0499	0.0265
98-04-14	0.033	0.042	0.034	0.0268	0.031	0.02	0.0268
98-04-16	0.14234	0.104	0.01029	0.0285	0.0556	0.034	0.0085
98-04-18	0.06	0.054	0.04	0.0398	0.048	0.037	0.0198
98-04-30	0.10798	0.10544	0.1029	0.0065	0.0923	0.0504	0.0165
	0.103	0.045	0.025	0.021	0.034	0.026	0.019

## 16. b,c system

	raw water	flotation	filtration	chloration	CGS	SE DAF	Slow sand	chloration
98-07-30	12.167	1.20	0.534	0.352	3.71	0.353	0.185	0.184
98-08-25	13.47	0.959	0.177	0.683	1.543	0.685	0.311	0.310
98-08-30	11.24	1.18	0.792	0.693	2.72	0.669	0.305	0.303
98-09-10	23.791	0.649	0.22	0.204	2.13	0.255	0.115	0.114
98-09-27	12.276	0.988	0.421	0.319	3.02	0.335	0.142	0.142
98-10-05	14.18	0.784	0.456	0.301	17.23	0.292	0.274	0.274
98-10-30	8.978	1.84	0.514	0.027	4.08	0.016	0.014	0.012
98-11-05	4.21	2.31	0.424	0.252	3.79	0.261	0.102	0.101
98-11-25	9.338	0.345	0.019	0.437	1.03	0.428	0.208	0.205
98-12-15	4.306	1.07	0.226	0.489	5.44	0.492	0.245	0.239
	4.21	0.649	0.019	0.027	1.03	0.016	0.014	0.012
	11.39	1.13	0.37	0.37	4.46	0.37	0.19	0.18
	23.791	2.31	0.792	0.683	17.23	0.685	0.311	0.310

17. b,c system UV-254

	raw water	flotation	filtration	chloriation	CGS	SE DAF	Slow sand	chloriation
98-07-30	0.079	0.057	0.054	0.054	0.071	0.052	0.048	0.038
98-08-25	0.077	0.054	0.053	0.052	0.068	0.051	0.037	0.016
98-08-30	0.068	0.053	0.052	0.050	0.162	0.048	0.032	0.011
98-09-10	0.065	0.052	0.050	0.048	0.062	0.046	0.030	0.030
98-09-27	0.066	0.052	0.051	0.047	0.053	0.043	0.034	0.028
98-10-05	0.066	0.055	0.049	0.047	0.045	0.041	0.028	0.028
98-10-30	0.083	0.054	0.053	0.052	0.051	0.039	0.028	0.017
98-11-05	0.077	0.052	0.051	0.044	0.076	0.041	0.031	0.016
98-11-25	0.071	0.052	0.052	0.050	0.056	0.048	0.029	0.017
98-12-15	0.058	0.054	0.053	0.052	0.051	0.047	0.031	0.024
	0.058	0.052	0.049	0.044	0.045	0.039	0.028	0.011
	0.070	0.050	0.050	0.040	0.060	0.040	0.032	0.021
	0.083	0.057	0.054	0.054	0.162	0.052	0.048	0.038

18. b,c system a

	raw water	flotation	filtration	chloriation	CGS	SE DAF	Slow sand	chloriation
98-07-30	15.201	0.742	0.481	0.280	12.167	0.037	0.036	0.031
98-08-25	15.88	3.776	0.251	0.192	13.475	0.198	0.181	0.120
98-08-30	19.12	0.044	0.974	0.478	11.242	0.477	0.0451	0.031
98-09-10	27.15	7.227	0.007	0.002	23.791	0.001	0.001	0.001
98-09-27	26.69	0.847	0.766	0.467	11.276	0.411	0.039	0.035
98-10-05	16.87	0.884	0.043	0.014	14.184	0.012	0.010	0.001
98-10-30	11.189	0.223	0.450	0.442	8.878	0.038	0.031	0.030
98-11-05	9.299	0.364	0.325	0.306	4.111	0.211	0.190	0.182
98-11-25	16.513	0.037	0.441	0.142	9.338	0.131	0.012	0.112
98-12-15	11.148	0.691	0.223	0.024	3.306	0.021	0.011	0.011
	9.299	0.037	0.007	0.002	3.306	0.001	0.001	0.001
	16.90	1.48	0.39	0.23	11.17	0.15	0.05	0.05
	27.15	7.227	0.974	0.478	23.791	0.477	0.190	0.182

19. b,c system KMnO

	raw water	flotation	filtration	chloriation	CGS	SE DAF	Slow sand	chloriation
98-07-30	4.792	4.210	1.264	1.172	4.424	1.152	1.113	1.021
98-08-25	2.624	2.149	1.611	1.911	2.344	1.876	1.245	1.010
98-08-30	5.095	5.012	4.231	3.933	6.752	4.011	2.853	2.210
98-09-10	7.781	4.497	3.942	3.821	4.678	3.815	2.325	1.987
98-09-27	5.343	3.655	2.984	2.084	5.191	2.101	1.987	0.999
98-10-05	7.342	3.963	2.892	2.723	5.431	2.811	2.652	2.541
98-10-30	3.791	0.284	0.124	0.369	3.825	0.361	0.311	0.310
98-11-05	1.931	0.796	0.431	0.851	0.953	0.814	0.784	0.699
98-11-25	2.592	1.060	0.785	0.792	1.912	0.801	0.659	0.641
98-12-15	4.631	0.894	0.561	0.461	0.937	0.215	0.395	0.351
	1.931	0.284	0.124	0.369	0.937	0.215	0.311	0.310
	4.59	2.65	1.88	1.81	3.64	1.79	1.43	1.17
	7.781	5.012	4.231	3.933	6.752	4.011	2.853	2.541

20. b,c system Zn

	raw water	flotation	filtration	chloriation	CGS	SE DAF	Slow sand	chloriation
98-07-30	0.063	0.022	0.012	0.004	0.055	0.013	0.012	0.001
98-08-25	0.021	0.0036	0.017	0.004	0.005	0.015	0.014	0.011
98-08-30	0.003	0.0028	0.0018	0.0019	0.001	0.0014	0.0013	0.001
98-09-10	0.004	0.0058	0.0051	0.003	0.001	0.004	0.0039	0.0029
98-09-27	0.199	0.0096	0.008	0.032	0.003	0.007	0.0066	0.005
98-10-05	0.003	0.003	0.002	0.0018	0.018	0.002	0.001	0.001
98-10-30	0.007	0.0032	0.0031	0.0023	0.004	0.003	0.002	0.001
98-11-05	0.007	0.0040	0.0032	0.0043	0.069	0.0029	0.002	0.001
98-11-25	0.006	0.0041	0.003	0.004	0.0038	0.003	0.002	0.0012
98-12-15	0.031	0.007	0.024	0.027	0.028	0.0022	0.0019	0.0018
	0.003	0.0028	0.0018	0.0018	0.001	0.0014	0.001	0.001
	0.034	0.006	0.007	0.008	0.018	0.005	0.004	0.002
	0.199	0.022	0.024	0.032	0.069	0.015	0.014	0.011

21. b,c system TOC

	raw water	flotation	filtration	chloriation	CGS	SE DAF	Slow sand	chloriation
98-07-30	2.376	1.985	0.768	0.564	0.985	0.551	0.441	0.440
98-08-25	3.277	1.092	0.883	0.511	0.891	0.499	0.369	0.336
98-08-30	1.243	1.064	0.986	0.617	0.617	0.521	0.421	0.412
98-09-10	2.021	1.893	1.844	1.973	1.973	1.023	0.985	0.788
98-09-27	2.776	1.84	1.751	1.824	1.821	1.623	1.123	1.121
98-10-05	2.717	1.887	1.316	1.691	1.693	1.429	1.112	1.001
98-10-30	1.342	1.278	1.164	1.131	1.351	1.017	0.965	0.945
98-11-05	2.029	1.898	1.847	1.971	1.770	1.349	0.899	0.771
98-11-25	2.777	1.813	1.753	1.824	1.921	1.542	1.231	1.114
98-12-15	2.754	1.884	1.314	1.697	1.793	1.667	1.521	1.489
	1.243	1.064	0.768	0.511	0.617	0.499	0.369	0.336
	2.33	1.66	1.36	1.38	1.48	1.12	0.90	0.84
	3.277	1.985	1.847	1.973	1.973	1.667	1.521	1.489

22. b,c system Mn

	raw water	flotation	filtration	chloriation	CGS	SE DAF	Slow sand	chloriation
98-07-30	0.196	0.006	0.004	0.0023	0.059	0.0023	0.001	0.001
98-08-25	0.017	0.017	0.004	0.002	0.018	0.002	0.001	0.001
98-08-30	0.009	0.012	0.005	0.007	0.03	0.0056	0.0031	0.0021
98-09-10	0.028	0.014	0.02	0.012	0.024	0.011	0.001	0.001
98-09-27	0.03	0.019	0.023	0.024	0.032	0.020	0.011	0.001
98-10-05	0.083	0.043	0.054	0.037	0.081	0.021	0.015	0.009
98-10-30	0.035	0.0324	0.02	0.0291	0.0341	0.022	0.017	0.008
98-11-05	0.6062	0.0398	0.0499	0.0265	0.0074	0.019	0.016	0.011
98-11-25	0.033	0.031	0.02	0.0268	0.042	0.0254	0.0189	0.015
98-12-15	0.14234	0.0556	0.034	0.0085	0.104	0.0062	0.003	0.001
	0.009	0.006	0.004	0.002	0.0074	0.002	0.001	0.001
	0.1179	0.0269	0.0233	0.0175	0.0431	0.0134	0.0087	0.0050
	0.6062	0.0556	0.054	0.037	0.104	0.0254	0.0189	0.015



23. b,c system Cu

	raw water	flotation	filtration	chloriation	CGS	SE DAF	Slow sand	chloriation
98-07-30	0.017	0.005	0.013	0.01	0.017	0.006	0.001	0.001
98-08-25	0.0017	0.0008	0.001	0.0012	0.0010	0.001	0.001	0.0005
98-08-30	0.0003	0.001	0.0005	0.0013	0.0002	0.0003	0.0002	0.0001
98-09-10	0.0008	0.0007	0.0006	0.0009	0.0006	0.0006	0.0005	0.0004
98-09-27	0.0008	0.0004	0.0008	0.0008	0.0007	0.0007	0.0007	0.0006
98-10-05	0.0013	0.0005	0.0011	0.0009	0.0010	0.0008	0.004	0.0034
98-10-30	0.0007	0.0007	0.0007	0.0011	0.0004	0.0001	0.0001	0.0001
98-11-05	0.0016	0.011	0.0013	0.0015	0.0006	0.0005	0.0009	0.0006
98-11-25	0.0012	0.0008	0.0008	0.0007	0.0012	0.0009	0.0007	0.0005
98-12-15	0.00278	0.00212	0.0012	0.00159	0.00078	0.0005	0.0006	0.0005
	0.0003	0.0004	0.0005	0.0007	0.0002	0.0001	0.0001	0.0001
	0.0028	0.0023	0.0021	0.0019	0.0023	0.0011	0.0009	0.0007
	0.017	0.011	0.013	0.01	0.017	0.006	0.004	0.0034

24. b,c system Fe

	raw water	flotation	filtration	chloriation	CGS	SE DAF	Slow sand	chloriation
98-07-30	0.435	0.093	0.079	0.077	0.219	0.080	0.060	0.050
98-08-25	0.249	0.175	0.026	0.103	0.226	0.028	0.022	0.021
98-08-30	0.151	0.151	0.026	0.056	0.078	0.024	0.019	0.011
98-09-10	0.315	0.092	0.048	0.087	0.229	0.044	0.038	0.025
98-09-27	0.195	0.057	0.033	0.874	0.074	0.0023	0.0021	0.0018
98-10-05	0.324	0.132	0.097	0.179	0.099	0.089	0.077	0.069
98-10-30	0.525	0.249	0.116	0.162	0.219	0.091	0.041	0.021
98-11-05	1.583	0.156	0.194	0.179	0.249	0.099	0.060	0.046
98-11-25	0.329	0.052	0.002	0.003	0.125	0.002	0.001	0.0005
98-12-15	0.193	0.114	0.101	0.031	0.178	0.098	0.009	0.005
	0.151	0.052	0.002	0.003	0.074	0.002	0.001	0.0005
	0.42	0.12	0.07	0.17	0.16	0.05	0.03	0.02
	1.583	0.249	0.194	0.874	0.249	0.099	0.077	0.069

- Abstract -

**A study on the water purification characteristics  
among the conventional sedimentation, circular-type  
dissolved air flotation and the combined process of  
sedimentation-flotation.**

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Wha Do Water Treatment Plant in City of Nam-Yang Ju located at Kyung-Ki Do in Korea has provided conventional water treatment process for over 20 years. The main source of water comes from Northern Han River, which flows from the northeast inland to west seashore of the Korean peninsula. The water qualities have been varied season to season. Sometimes, it is prone to bring about algal blooms and flash turbidity spikes exceeding 100 NTU in heavy rainy seasons. Though the water qualities have changed with times and seasons, the water treatment

process has unchanged from the original design: coagulation, sedimentation, slow-speed sand filtration and chlorination.

Recently, it was proved that the conventional plant has a limitation in improving the performance, then the dissolved air flotation (DAF), having circular type DAF which contained sand filter (named as sand-DAF), was adapted as the best process for updating treated water quality and solving construction costs. And also the sedimentation basin was reconstructed with the series process of sedimentation-DAF (named as sedi-flotation process). Sedimentation works with a steady capacity of 6000 m<sup>3</sup>/day and sand-DAF with 6000 m<sup>3</sup>/day.

The sedi-DAF, 6000 m<sup>3</sup>/day, were designed and installed in the rear of the rectangular sedimentation basin. The sedimentation tank, 4,000 m<sup>3</sup>/day, had an inclined plate at the middle side moved to back and forth. The pre-treatment systems were coagulant dosing devices, rapid mixing tank, flocculator with baffled channel. The DAF systems consist of air dissolving tube, depressurizing nozzles, scum removal devices. Those DAF systems were the generalized-style of the DAF system except the air dissolving tube (ADT). Though the retention time in the ADT unit was so short as 19 seconds, we successfully made fine-bubbles at the flotation zone.

In this study, we mainly compared the removal efficiency for turbidity with the variations of raw water turbidity. And also measured the KMnO<sub>4</sub> consumption, UV<sub>254</sub>, TOC, Fe, Mn, chlorophyll-a reduction

for sand-DAF, sedi-flotation process.

In the long run, the conventional sedimentation and circular-DAF process seemed to treat the water within the Korean standards. But it was obtained that circular-DAF process showed a litter higher efficiencies in turbidity, TOC, UV254, Fe, Mn removal. We, therefore, conclude that circular-DAF system should have substantial advantages over conventional process in all matters.

During the study period, it was also clearly showed that sedi-DAF effluent have a higher removal efficiencies than those of the sedimentation in the TOC, UV254, chlorophyll-a. And the effluent concentrations of the sedi-DAF were 0.9 – 3.8mg/L in TOC, 0.058 – 0.08 abs./cm in UV254, 0.5 – 3.3 mg/ m<sup>3</sup>, each of them.

From the above results, we could be certified that the sedi-DAF had a good efficiency in TOC, UV254, and chlorophyll-a removal, so it was a successful trial that the combination of a sedimentation and DAF process.

After 6 months of operation period, it was found that the filter run time was prolonged from 5 days to 10 – 12 days in the sedi-DAF system. Especially, the times when chlorophyll-a concentration was very high, the effects of sedi-DAF were precisely revealed in the filter run time.